

The S-8340/8341 Series is a CMOS step-up switching regulator controller which mainly consists of a reference voltage source, oscillation circuit, error amplifier, phase compensation circuit, PWM control circuit (S-8340 Series), and PWM/PFM switching control circuit (S-8341 Series).

Since the oscillation frequency is a high 300 kHz or 600 kHz, with the addition of a small external part, the S-8340/8341 Series functions as a highly efficient step-up switching regulator with a high output current. The speed of the output stage is enhanced so that the N-channel power MOS with a low on-resistance can be switched quickly.

The S-8340 Series realizes low ripple, high efficiency, and excellent transient characteristics thanks to a PWM control circuit capable of varying the duty ratio linearly from 0 to 82%, optimized error amplifier, and phase compensation circuit.

The S-8341 Series contains a PWM/PFM switching control circuit so that it operates using PWM control with a duty ratio of 27% or higher and using PFM control with a duty ratio of lower than 27% to ensure high efficiency in all load ranges.

These S-8340/8341 Series serve as ideal main power supply units for portable devices when coupled with the 8-Pin TSSOP package and high oscillation frequencies.

Oscillation frequency : 600 kHz (A and B types), 300 kHz (C and D types).  
Output voltage : Selectable in 0.1 V steps between 2.5 to 6.0 V (output voltage fixed output type)  
Output voltage accuracy : 2.0%  
Output voltage external setting (FB) type available. FB terminal voltage ( $V_{FB}$ ) 1.0 V  
External parts : Coil, diode, capacitors (3), transistor, and resistor only  
Duty ratio : 0 to 82% (typ.) PWM control (S-8340 Series)  
27 to 82% (typ.) PWM/PFM switching control (S-8341 Series A and B types)  
21 to 82% (typ.) PWM/PFM switching control (S-8341 Series C and D types)  
Low-voltage operation: Oscillation guaranteed to start when  $V_{DD}$  0.9 V  
Built-in current limit circuit: Can be set with an external resistor ( $R_{SENSE}$ )  
Soft-start function set by an external capacitor ( $C_{SS}$ )  
Shutdown function  
Lead-free, Sn 100%, halogen-free

Refer to “ ” for details.

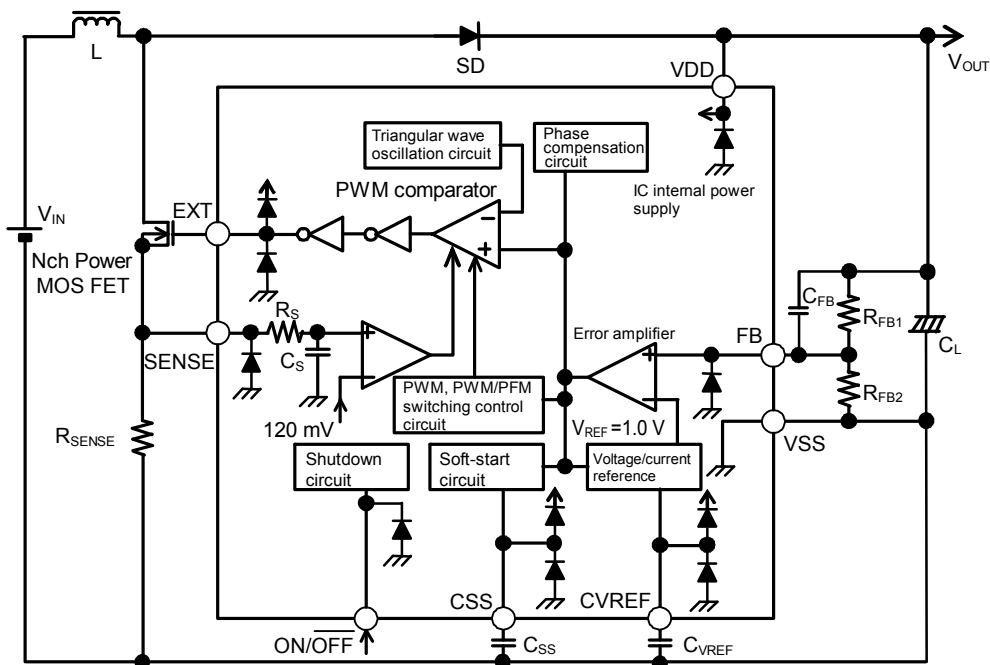
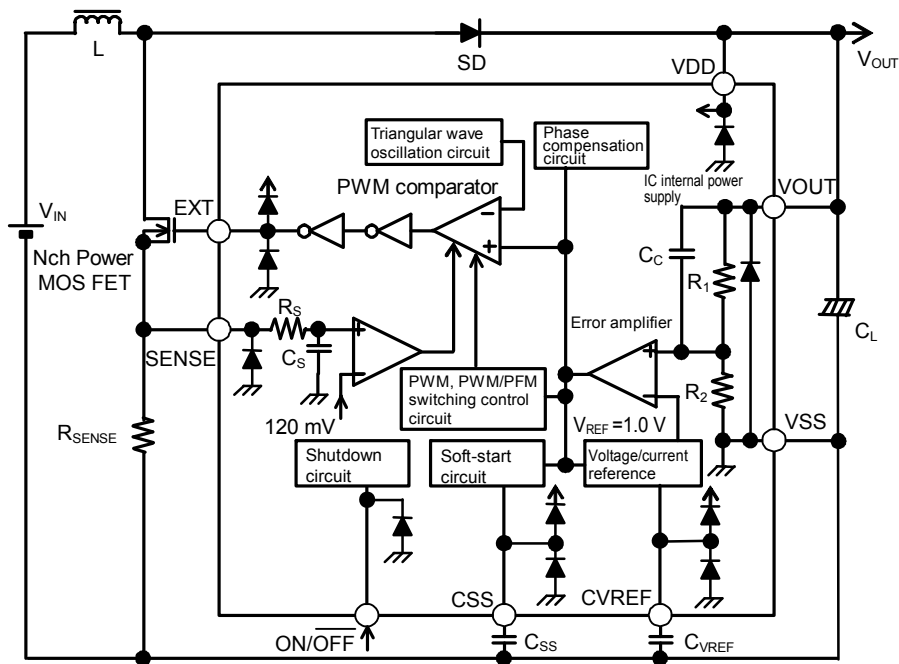
Power supplies for portable equipments such as PDAs, electronic notebooks, and cellular phones

Power supplies for audio equipments such as portable CD players, portable MD players, and headphone stereos

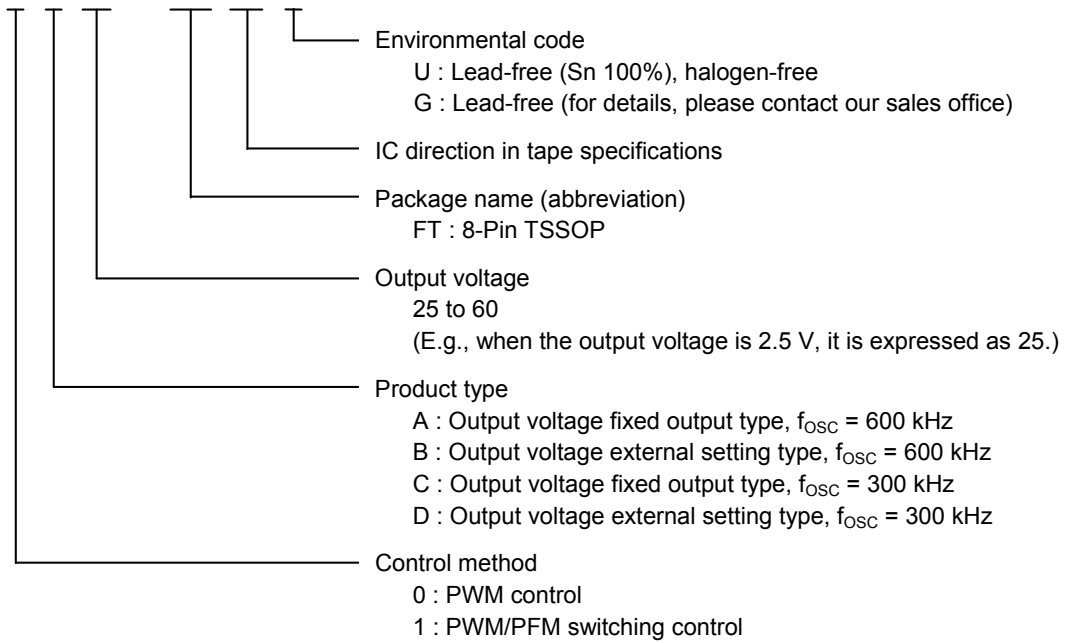
Main or local power supplies for notebook PCs and peripherals

Constant voltage power supplies for cameras, VCRs, and communication devices

8-Pin TSSOP



The control method, product type, and output voltage values for the S-8340/8341 Series can be selected depending on usage. Refer to “ ” for the definition of the product name, “ ” regarding the package drawings and “ ” for the full product names.



Refer to the tape drawing.

Package Name		Drawing Code		
		Package	Tape	Reel
8-Pin TSSOP	Environmental code = G	FT008-A-P-SD	FT008-E-C-SD	FT008-E-R-SD
	Environmental code = U	FT008-A-P-SD	FT008-E-C-SD	FT008-E-R-S1

Output Voltage (V)	S-8340 Series A Type $f_{OSC} = 600$ kHz PWM Control	S-8341 Series A Type $f_{OSC} = 600$ kHz PWM/PFM Switching Control	S-8340 Series C Type $f_{OSC} = 300$ kHz PWM Control	S-8341 Series C Type $f_{OSC} = 300$ kHz PWM/PFM Switching Control
2.5 V	S-8340A25AFT-T2-x	S-8341A25AFT-T2-x	S-8340C25AFT-T2-x	S-8341C25AFT-T2-x
3.0 V	S-8340A30AFT-T2-x	S-8341A30AFT-T2-x	S-8340C30AFT-T2-x	S-8341C30AFT-T2-x
3.3 V	S-8340A33AFT-T2-x	S-8341A33AFT-T2-x	S-8340C33AFT-T2-x	S-8341C33AFT-T2-x
3.4 V	S-8340A34AFT-T2-x			
3.5 V	S-8340A35AFT-T2-x			
5.0 V	S-8340A50AFT-T2-x	S-8341A50AFT-T2-x	S-8340C50AFT-T2-x	S-8341C50AFT-T2-x
5.1 V	S-8340A51AFT-T2-x			S-8341C51AFT-T2-x
5.6 V	S-8340A56AFT-T2-x			
6.0 V	S-8340A60AFT-T2-x		S-8340C60AFT-T2-x	

Contact the ABLIC Inc. marketing department for products with an output voltage other than those specified above.

x: G or U

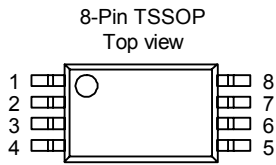
Please select products of environmental code = U for Sn 100%, halogen-free products.

Output Voltage (V)	S-8340 Series B Type $f_{OSC} = 600$ kHz PWM Control	S-8341 Series B Type $f_{OSC} = 600$ kHz PWM/PFM Switching Control	S-8340 Series D Type $f_{OSC} = 300$ kHz PWM Control	S-8341 Series D Type $f_{OSC} = 300$ kHz PWM/PFM Switching Control
External setting	S-8340B00AFT-T2-x	S-8341B00AFT-T2-x	S-8340D00AFT-T2-x	S-8341D00AFT-T2-x

x: G or U

Please select products of environmental code = U for Sn 100%, halogen-free products.

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Pin No.	Symbol	Pin Description
1	VSS	GND pin
2	CVREF	Reference voltage source pass capacitor connection pin
3	CSS	Soft-start capacitor connection pin
4	ON/ $\overline{\text{OFF}}$	Shutdown pin "H" : Normal operation (step-up operating) "L" : Entire circuit stopped (step-up stopped)
5	VDD	IC power supply pin
6	VOUT (FB)	Output voltage fixed output type : Output voltage monitoring pin [Output voltage external setting type : Feedback pin]
7	EXT	External transistor connection pin
8	SENSE	Current limit detection pin

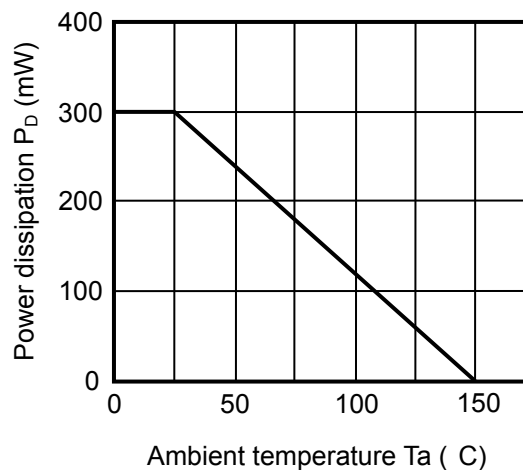
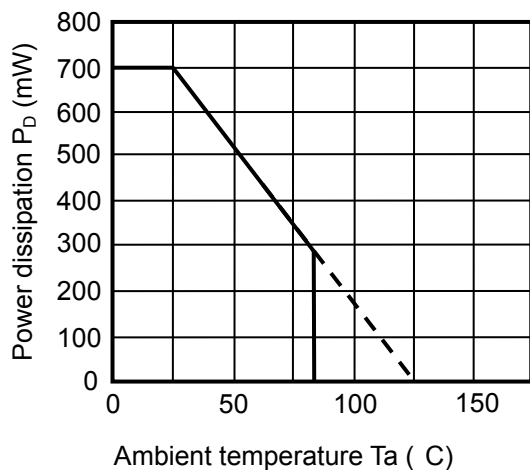
(Ta = 25 C unless otherwise specified)

Parameter	Symbol	Absolute Maximum Rating	Unit
VDD pin voltage	$V_{DD}$	$V_{SS} - 0.3$ to $V_{SS} + 12$	V
VOOUT pin voltage	$V_{OUT}$	$V_{SS} - 0.3$ to $V_{SS} + 12$	V
FB pin voltage	$V_{FB}$	$V_{SS} - 0.3$ to $V_{SS} + 12$	V
CVREF pin voltage	$V_{CVREF}$	$V_{SS} - 0.3$ to $V_{DD} + 0.3$	V
CSS pin voltage	$V_{CSS}$	$V_{SS} - 0.3$ to $V_{DD} + 0.3$	V
ON/OFF pin voltage	$V_{ON/OFF}$	$V_{SS} - 0.3$ to $V_{SS} + 12$	V
SENSE pin voltage	$V_{SENSE}$	$V_{SS} - 0.3$ to $V_{SS} + 12$	V
EXT pin voltage	$V_{EXT}$	$V_{SS} - 0.3$ to $V_{DD} + 0.3$	V
EXT pin current	$I_{EXT}$	100	mA
Power dissipation	$P_D$	300 (When not mounted on board)	mW
		700	mW
Operating ambient temperature	$T_{dpr}$	40 to 85	C
Storage temperature	$T_{stg}$	40 to 125	C

When mounted on board

[Mounted board]

- (1) Board size : 114.3 mm × 76.2 mm × t1.6 mm
- (2) Board name : JEDEC STANDARD51-7



(Ta = 25 C unless otherwise specified)

Parameter	Symbol	Conditions	Min.	Typ.	Max.	Unit	Measurement Circuit	
Output voltage	$V_{OUT(E)}$	$V_{IN}$ $V_{OUT(S)}$ 0.6, $I_{OUT}$ $V_{OUT(S)}/50$ :	$V_{OUT(S)}$ 0.98	$V_{OUT(S)}$	$V_{OUT(S)}$ 1.02	V	1	
Input voltage	$V_{IN}$				6	V	1	
Oscillation start voltage	$V_{ST}$	No external parts. The voltage is applied to $V_{OUT}$ .			0.9	V	2	
Current consumption 1	$I_{SS1}$	$V_{OUT}$ $V_{OUT(S)}$ 0.95, EXT pin open	S-834xA25 34	350	640	A	2	
			S-834xA35 44	460	810	A	2	
			S-834xA45 54	630	1060	A	2	
			S-834xA55 60	810	1250	A	2	
Current consumption 2	$I_{SS2}$	$V_{OUT}$ $V_{OUT(S)}$ 0.5 V, EXT pin open		180	300	A	2	
Current consumption at shutdown	$I_{SS3}$	$V_{OUT}$ $V_{OUT(S)}$ 0.95, $V_{ON/OFF}$ 0 V			3.0	A	2	
EXT pin output current	$I_{EXTH}$	$V_{EXT}$ $V_{OUT(E)}$ 0.2 V	S-834xA25 34	13	24		mA	
			S-834xA35 44	17	30		mA	
			S-834xA45 54	21	34		mA	
			S-834xA55 60	23	37		mA	
	$I_{EXTL}$	$V_{EXT}$ 0.2 V	S-834xA25 34	32	56		mA	
			S-834xA35 44	42	69		mA	
			S-834xA45 54	50	78		mA	
			S-834xA55 60	56	85		mA	
Line regulation	$V_{OUT1}$	$V_{IN}$ $V_{OUT(S)}$ 0.4 to $V_{OUT(S)}$ 0.6 $I_{OUT}$ $V_{OUT(S)}/50$ :		$V_{OUT(S)}$ 0.5%	$V_{OUT(S)}$ 1%	V	1	
Load regulation	$V_{OUT2}$	$V_{IN}$ $V_{OUT(S)}$ 0.6, 10 A $I_{OUT}$ $V_{OUT(S)}/40$ :		$V_{OUT(S)}$ 0.5%	$V_{OUT(S)}$ 1%	V	1	
Output voltage temperature coefficient	$\frac{V_{OUT}}{Ta}$	$V_{IN}$ $V_{OUT(S)}$ 0.6, $I_{OUT}$ $V_{OUT(S)}/50$ : , $Ta$ 40 to 85 C		100		ppm/ C	1	
Oscillation frequency	$f_{OSC}$	$V_{OUT}$ $V_{OUT(S)}$ 0.95 Measure waveform at the EXT pin	510	600	690	kHz	2	
Maximum duty ratio	MaxDuty	$V_{IN}$ $V_{OUT(S)}$ 0.95 Measure waveform at the EXT pin	73	82	89	%	2	
PWM/PFM switching duty ratio (S-8341 Series A type)	PFMDuty	$V_{IN}$ $V_{OUT(E)}$ 0.1 V, under no load	19	27	35	%	1	
Current limit detection voltage	$V_{SENSE}$	$V_{OUT}$ $V_{OUT(S)}$ 0.95 Judge oscillation at the EXT pin or oscillation stop at "L"	90	120	150	mV	2	
ON/OFF pin input voltage	$V_{SH}$	$V_{OUT}$ $V_{OUT(S)}$ 0.95 Judge oscillation at the EXT pin.	0.8			V	2	
	$V_{SL}$	$V_{OUT}$ $V_{OUT(S)}$ 0.95 Judge oscillation stop at the EXT pin.			0.3	V	2	
ON/OFF pin input leakage current	$I_{SH}$	$V_{OUT}$ 6 V, $V_{ON/OFF}$ 6 V	0.1		0.1	A	2	
	$I_{SL}$	$V_{OUT}$ 6 V, $V_{ON/OFF}$ 0 V	0.1		0.1	A	2	
Soft-start time	$t_{SS}$	$V_{IN}$ $V_{OUT(S)}$ 0.6, $C_{SS}$ 4700 pF, $I_{OUT}$ $V_{OUT(S)}/50$ : Measure time until oscillation occurs at the EXT pin.	S-8340Axx	3.0	6.0	14.0	ms	1
			S-8341Axx	3.0	8.0	14.0	ms	1
Efficiency	EFFI	$V_{IN}$ $V_{OUT(S)}$ 0.6, $I_{OUT}$ $V_{OUT(S)}/50$ :	S-834xA25 34	83			%	1
			S-834xA35 44	85			%	1
			S-834xA45 54	87			%	1
			S-834xA55 60	87			%	1

External parts	Coil :	Sumida Corporation CD54 (10 H)
	Diode :	Matsushita Electronic Industrial Co., Ltd. MA735 (Schottky type)
	Capacitor :	Nichicon Corporation F93 (16 V, 47 F, tantalum type)
	Transistor :	Sanyo Electric Co., Ltd. 2SD1628G
	Base resistor (R <sub>b</sub> ) :	1.0 k :
	Base capacitor (C <sub>b</sub> ) :	2200 pF (ceramic type)
	C <sub>VREF</sub> :	0.01 F
	C <sub>SS</sub> :	4700 pF

The VDD pin is connected to the VOUT pin.

The ON/OFF pin is connected to the VOUT pin unless otherwise specified.

Connect the SENSE pin to the VSS pin.

V<sub>OUT(S)</sub> : Set output voltage value

V<sub>OUT(E)</sub> : Actual output voltage value : Output voltage value when I<sub>OUT</sub> = V<sub>OUT(S)</sub>/50 : and V<sub>IN</sub> = V<sub>OUT(S)</sub> + 0.6.

The change of output voltage with temperature [mV/ C] is calculated from the following formula.

$$\frac{V_{OUT}}{T_a} \text{ [mV/ C]} = V_{OUT(S)} \text{ [V]} \cdot \frac{V_{OUT}}{T_a} \text{ [ppm/ C]} \cdot 1000$$

(Change of output voltage with temperature) (Set output voltage value) (Output voltage temperature coefficient)



(Ta = 25 C unless otherwise specified)

Parameter	Symbol	Conditions	Min.	Typ.	Max.	Unit	Measurement Circuit	
Output voltage	$V_{OUT(E)}$	$V_{IN}$ 2.4 V, $I_{OUT}$ 80 mA	3.920	4.000	4.080	V	3	
FB pin voltage	$V_{FB}$	$V_{IN}$ 2.4 V, $I_{OUT}$ 80 mA	0.980	1.000	1.020	V	3	
Input voltage	$V_{IN}$				6	V	3	
Oscillation start voltage	$V_{ST2}$	No external parts. The voltage is applied to $V_{DD}$ .			0.9	V	4	
Current consumption 1	$I_{SS1}$	$V_{OUT}$ 3.8 V		460	740	A	4	
Current consumption 2	$I_{SS2}$	$V_{OUT}$ 4.5 V		180	300	A	4	
Current consumption at shutdown	$I_{SSS}$	$V_{OUT}$ 3.8 V, $V_{ON/OFF}$ 0 V			3.0	A	4	
EXT pin output current	$I_{EXTH}$	$V_{EXT}$ $V_{OUT(E)}$ 0.2 V	19	30		mA		
	$I_{EXTL}$	$V_{EXT}$ 0.2 V	46	69		mA		
Line regulation	$V_{OUT1}$	1.6 V $V_{IN}$ 2.4 V, $I_{OUT}$ 80 mA		20	40	mV	3	
Load regulation	$V_{OUT2}$	$V_{IN}$ 2.4 V, 10 A $I_{OUT}$ 100 mA		20	40	mV	3	
Output voltage temperature coefficient	$\frac{V_{OUT}}{Ta V_{OUT}}$	$V_{IN}$ 2.4 V, $I_{OUT}$ 80 mA, $Ta$ 40 to 85°C		100		ppm/°C	3	
Oscillation frequency	$f_{OSC}$	$V_{OUT}$ 3.8 V, measure waveform at the EXT pin	510	600	690	kHz	4	
Maximum duty ratio	MaxDuty	$V_{IN}$ 3.8 V, measure waveform at the EXT pin	73	82	89	%	4	
PWM/PFM switching duty ratio (S-8341 Series B type)	PFMDuty	$V_{IN}$ $V_{OUT(E)}$ 0.1 V, under no load	19	27	35	%	3	
Current limit detection voltage	$V_{SENSE}$	$V_{OUT}$ 3.8 V Judge oscillation at the EXT pin or oscillation stop at "L"	90	120	150	mV	4	
FB pin input current	$I_{FB}$	$V_{OUT}$ 6 V, $V_{FB}$ 1.5 V	50		50	nA	4	
ON/OFF pin input voltage	$V_{SH}$	$V_{OUT}$ 3.8 V Judge oscillation at the EXT pin.	0.8			V	4	
	$V_{SL}$	$V_{OUT}$ 3.8 V Judge oscillation stop at the EXT pin.			0.3	V	4	
ON/OFF pin input leakage current	$I_{SH}$	$V_{OUT}$ 6 V, $V_{ON/OFF}$ 6 V	0.1		0.1	A	4	
	$I_{SL}$	$V_{OUT}$ 6 V, $V_{ON/OFF}$ 0 V	0.1		0.1	A	4	
Soft-start time	$t_{SS}$	$V_{IN}$ 2.4 V, $C_{SS}$ 4700 pF, $I_{OUT}$ 80 mA, Measure time until oscillation occurs at the EXT pin.	S-8340B00	3.0	6.0	14.0	ms	3
			S-8341B00	3.0	8.0	14.0	ms	3
Efficiency	EFF1	$V_{IN}$ 2.4 V, $I_{OUT}$ 80 mA		85		%	3	

External parts	Coil :	Sumida Corporation CD54 (10 H)
	Diode :	Matsushita Electronic Industrial Co., Ltd. MA735 (Schottky type)
	Capacitor :	Nichicon Corporation F93 (16 V, 47 F, tantalum type)
	Transistor :	Sanyo Electric Co., Ltd. 2SD1628G
	Base resistor ( $R_b$ ) :	1.0 k :
	Base capacitor ( $C_b$ ) :	2200 pF (ceramic type)
	$C_{VREF}$ :	0.01 F
	$C_{SS}$ :	4700 pF
	$R_{FB1}$ :	300 k :
	$R_{FB2}$ :	100 k :
	$C_{FB}$ :	50 pF

The ON/OFF pin is connected to the VOUT pin unless otherwise specified.  
Connect the SENSE pin to the VSS pin.

$V_{OUT(E)}$  : Actual output voltage value : Output voltage value when  $I_{OUT} = 80$  mA and  $V_{IN} = 2.4$  V is applied.

The Typ. value (set output voltage value) is  $1 + \frac{300 \text{ k} :}{100 \text{ k} :}$  [V]

The change of output voltage with temperature [mV/ C] is calculated from the following formula. However, the temperature change rates for  $R_{FB1}$  and  $R_{FB2}$  are assumed to be the same.

$$\frac{V_{OUT}}{T_a} \text{ [mV/ C]} = 1 + \frac{R_{FB1}}{R_{FB2}} \cdot \frac{V_{OUT}}{T_a} \text{ [ppm/ C]} \cdot 1000$$

(Change of output voltage with temperature) (Set output voltage value) (Output voltage temperature coefficient)

(Ta = 25 C unless otherwise specified)

Parameter	Symbol	Conditions	Min.	Typ.	Max.	Unit	Measurement Circuit	
Output voltage	$V_{OUT(E)}$	$V_{IN}$ $V_{OUT(S)}$ 0.6, $I_{OUT}$ $V_{OUT(S)}/50$ :	$V_{OUT(S)}$ 0.98	$V_{OUT(S)}$	$V_{OUT(S)}$ 1.02	V	1	
Input voltage	$V_{IN}$				6	V	1	
Oscillation start voltage	$V_{ST}$	No external parts. The voltage is applied to $V_{OUT}$ .			0.9	V	2	
Current consumption 1	$I_{SS1}$	$V_{OUT}$ $V_{OUT(S)}$ 0.95, EXT pin open	S-834xC25 34	210	430	A	2	
			S-834xC35 44	270	520	A	2	
			S-834xC45 54	350	650	A	2	
			S-834xC55 60	440	740	A	2	
Current consumption 2	$I_{SS2}$	$V_{OUT}$ $V_{OUT(S)}$ 0.5 V, EXT pin open		110	185	A	2	
Current consumption at shutdown	$I_{SSS}$	$V_{OUT}$ $V_{OUT(S)}$ 0.95, $V_{ON/OFF}$ 0 V			3.0	A	2	
EXT pin output current	$I_{EXTH}$	$V_{EXT}$ $V_{OUT(E)}$ 0.2 V	S-834xC25 34	13	24	mA		
			S-834xC35 44	17	30	mA		
			S-834xC45 54	21	34	mA		
			S-834xC55 60	23	37	mA		
	$I_{EXTL}$	$V_{EXT}$ 0.2 V	S-834xC25 34	32	56	mA		
			S-834xC35 44	42	69	mA		
			S-834xC45 54	50	78	mA		
			S-834xC55 60	56	85	mA		
Line regulation	$V_{OUT1}$	$V_{IN}$ $V_{OUT(S)}$ 0.4 to $V_{OUT(S)}$ 0.6 $I_{OUT}$ $V_{OUT(S)}/50$ :		$V_{OUT(S)}$ 0.5%	$V_{OUT(S)}$ 1%	V	1	
Load regulation	$V_{OUT2}$	$V_{IN}$ $V_{OUT(S)}$ 0.6, 10 A $I_{OUT}$ $V_{OUT(S)}/40$ :		$V_{OUT(S)}$ 0.5%	$V_{OUT(S)}$ 1%	V	1	
Output voltage temperature coefficient	$\frac{V_{OUT}}{Ta}$	$V_{IN}$ $V_{OUT(S)}$ 0.6, $I_{OUT}$ $V_{OUT(S)}/50$ : Ta 40 to 85 C		100		ppm/ C	1	
Oscillation frequency	$f_{OSC}$	$V_{OUT}$ $V_{OUT(S)}$ 0.95 Measure waveform at the EXT pin	255	300	345	kHz	2	
Maximum duty ratio	MaxDuty	$V_{IN}$ $V_{OUT(S)}$ 0.95 Measure waveform at the EXT pin	73	82	89	%	2	
PWM/PFM switching duty ratio (S-8341 Series C type)	PFMDuty	$V_{IN}$ $V_{OUT(E)}$ 0.1 V, under no load	15	21	31	%	1	
Current limit detection voltage	$V_{SENSE}$	$V_{OUT}$ $V_{OUT(S)}$ 0.95 Judge oscillation at the EXT pin or oscillation stop at "L"	90	120	150	mV	2	
ON/OFF pin input voltage	$V_{SH}$	$V_{OUT}$ $V_{OUT(S)}$ 0.95 Judge oscillation at the EXT pin.	0.8			V	2	
	$V_{SL}$	$V_{OUT}$ $V_{OUT(S)}$ 0.95 Judge oscillation stop at the EXT pin.			0.3	V	2	
ON/OFF pin input leakage current	$I_{SH}$	$V_{OUT}$ 6 V, $V_{ON/OFF}$ 6 V	0.1		0.1	A	2	
	$I_{SL}$	$V_{OUT}$ 6 V, $V_{ON/OFF}$ 0 V	0.1		0.1	A	2	
Soft-start time	$t_{SS}$	$V_{IN}$ $V_{OUT(S)}$ 0.6, $C_{SS}$ 4700 pF, $I_{OUT}$ $V_{OUT(S)}/50$ : , Measure time until oscillation occurs at EXT pin.	S-8340Cxx	6.0	14.3	28.0	ms	1
			S-8341Cxx	6.0	17.2	28.0	ms	1
Efficiency	EFFI	$V_{IN}$ $V_{OUT(S)}$ 0.6, $I_{OUT}$ $V_{OUT(S)}/50$ :	S-834xC25 34		83		%	1
			S-834xC35 44		85		%	1
			S-834xC45 54		87		%	1
			S-834xC55 60		87		%	1

External parts	Coil :	Sumida Corporation CD54 (10 H)
	Diode :	Matsushita Electronic Industrial Co., Ltd. MA735 (Schottky type)
	Capacitor :	Nichicon Corporation F93 (16 V, 47 F, tantalum type)
	Transistor :	Sanyo Electric Co., Ltd. 2SD1628G
	Base resistor (R <sub>b</sub> ) :	1.0 k :
	Base capacitor (C <sub>b</sub> ) :	2200 pF (ceramic type)
	C <sub>VREF</sub> :	0.01 F
	C <sub>SS</sub> :	4700 pF

The VDD pin is connected to the VOUT pin.

The ON/OFF pin is connected to the VOUT pin unless otherwise specified.

Connect the SENSE pin to the VSS pin.

V<sub>OUT(S)</sub> : Set output voltage value

V<sub>OUT(E)</sub> : Actual output voltage value : Output voltage value when I<sub>OUT</sub> = V<sub>OUT(S)</sub>/50 : and V<sub>IN</sub> = V<sub>OUT(S)</sub> + 0.6.

The change of output voltage with temperature [mV/ C] is calculated from the following formula.

$$\frac{V_{OUT}}{T_a} \text{ [mV/ C]} = V_{OUT(S)} \text{ [V]} \cdot \frac{V_{OUT}}{T_a} \text{ [ppm/ C]} \cdot 1000$$

(Change of output voltage with temperature) (Set output voltage value) (Output voltage temperature coefficient)

(Ta = 25 C unless otherwise specified)

Parameter	Symbol	Conditions	Min.	Typ.	Max.	Unit	Measurement Circuit	
Output voltage	$V_{OUT(E)}$	$V_{IN} = 2.4 \text{ V}$ , $I_{OUT} = 80 \text{ mA}$	3.920	4.000	4.080	V	3	
FB pin voltage	$V_{FB}$	$V_{IN} = 2.4 \text{ V}$ , $I_{OUT} = 80 \text{ mA}$	0.980	1.000	1.020	V	3	
Input voltage	$V_{IN}$				6	V	3	
Oscillation start voltage	$V_{ST2}$	No external parts. The voltage is applied to $V_{DD}$ .			0.9	V	4	
Current consumption 1	$I_{SS1}$	$V_{OUT} = 3.8 \text{ V}$		255	460	A	4	
Current consumption 2	$I_{SS2}$	$V_{OUT} = 4.5 \text{ V}$		110	185	A	4	
Current consumption at shutdown	$I_{SSS}$	$V_{OUT} = 3.8 \text{ V}$ , $V_{ON/OFF} = 0 \text{ V}$			3.0	A	4	
EXT pin output current	$I_{EXTH}$	$V_{EXT} = V_{OUT(E)} - 0.2 \text{ V}$	19	30		mA		
	$I_{EXTL}$	$V_{EXT} = 0.2 \text{ V}$	46	69		mA		
Line regulation	$V_{OUT1}$	1.6 V $V_{IN} = 2.4 \text{ V}$ , $I_{OUT} = 80 \text{ mA}$		20	40	mV	3	
Load regulation	$V_{OUT2}$	$V_{IN} = 2.4 \text{ V}$ , 10 A $I_{OUT} = 100 \text{ mA}$		20	40	mV	3	
Output voltage temperature coefficient	$\frac{V_{OUT}}{Ta V_{OUT}}$	$V_{IN} = 2.4 \text{ V}$ , $I_{OUT} = 80 \text{ mA}$ , $Ta = 40 \text{ to } 85^\circ\text{C}$		100		ppm/ $^\circ\text{C}$	3	
Oscillation frequency	$f_{OSC}$	$V_{OUT} = 3.8 \text{ V}$ , Measure waveform at the EXT pin	255	300	345	kHz	4	
Maximum duty ratio	MaxDuty	$V_{IN} = 3.8 \text{ V}$ , Measure waveform at the EXT pin	73	82	89	%	4	
PWM/PFM switching duty ratio (S-8341 Series D type)	PFMDuty	$V_{IN} = V_{OUT(E)} - 0.1 \text{ V}$ , Under no load	15	21	31	%	3	
Current limit detection voltage	$V_{SENSE}$	$V_{OUT} = 3.8 \text{ V}$ Judge oscillation at the EXT pin or oscillation stop at "L"	90	120	150	mV	4	
FB pin input current	$I_{FB}$	$V_{OUT} = 6 \text{ V}$ , $V_{FB} = 1.5 \text{ V}$	50		50	nA	4	
ON/OFF pin input voltage	$V_{SH}$	$V_{OUT} = 3.8 \text{ V}$ Judge oscillation at the EXT pin.	0.8			V	4	
	$V_{SL}$	$V_{OUT} = 3.8 \text{ V}$ Judge oscillation stop at the EXT pin.			0.3	V	4	
ON/OFF pin input leakage current	$I_{SH}$	$V_{OUT} = 6 \text{ V}$ , $V_{ON/OFF} = 6 \text{ V}$	0.1		0.1	A	4	
	$I_{SL}$	$V_{OUT} = 6 \text{ V}$ , $V_{ON/OFF} = 0 \text{ V}$	0.1		0.1	A	4	
Soft-start time	$t_{SS}$	$V_{IN} = 2.4 \text{ V}$ , $C_{SS} = 4700 \text{ pF}$ , $I_{OUT} = 80 \text{ mA}$ , Measure time until oscillation occurs at the EXT pin.	S-8340D00	6.0	14.3	28.0	ms	3
			S-8341D00	6.0	17.2	28.0	ms	3
Efficiency	EFFI	$V_{IN} = 2.4 \text{ V}$ , $I_{OUT} = 80 \text{ mA}$		85		%	3	

External parts	Coil :	Sumida Corporation CD54 (10 H)
	Diode :	Matsushita Electronic Industrial Co., Ltd. MA735 (Schottky type)
	Capacitor :	Nichicon Corporation F93 (16 V, 47 F, tantalum type)
	Transistor :	Sanyo Electric Co., Ltd. 2SD1628G
	Base resistor (R <sub>b</sub> ) :	1.0 k :
	Base capacitor (C <sub>b</sub> ) :	2200 pF (ceramic type)
	C <sub>VREF</sub> :	0.01 F
	C <sub>SS</sub> :	4700 pF
	R <sub>FB1</sub> :	300 k :
	R <sub>FB2</sub> :	100 k :
	C <sub>FB</sub> :	50 pF

The ON/OFF pin is connected to the VOUT pin unless otherwise specified.  
Connect the SENSE pin to the VSS pin.

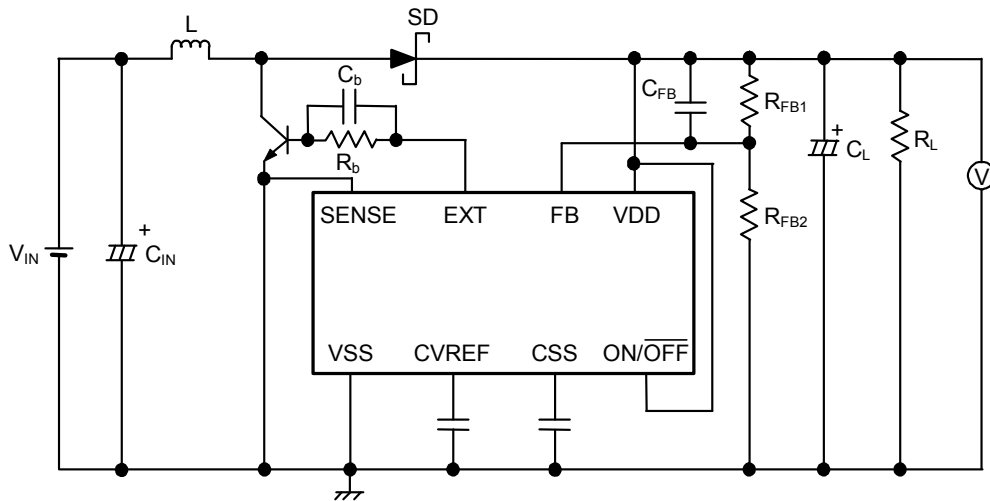
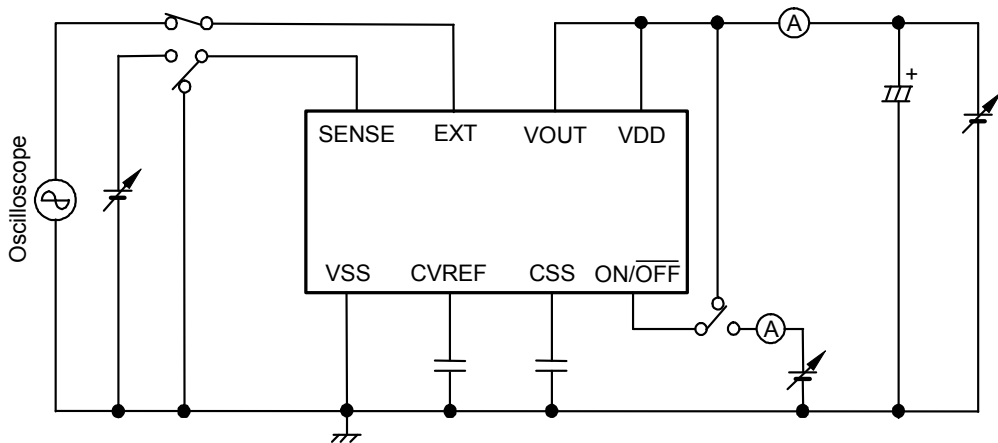
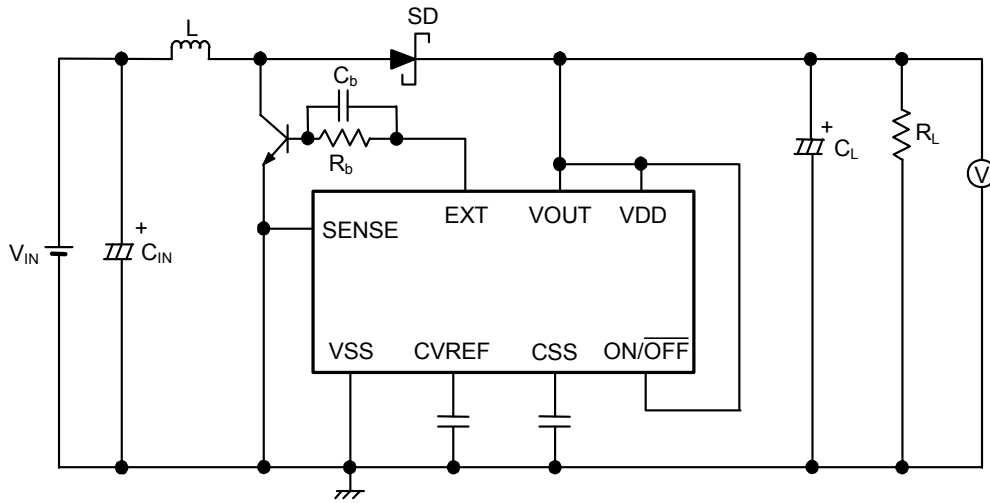
V<sub>OUT(E)</sub> : Actual output voltage value : Output voltage value when I<sub>OUT</sub> = 80 mA and V<sub>IN</sub> = 2.4 V is applied.

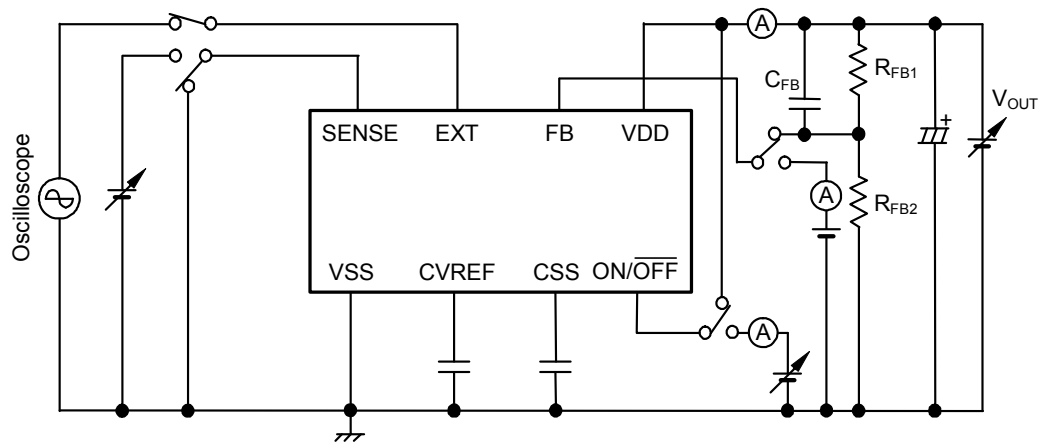
The Typ. value (set output voltage value) is  $1 + \frac{300 \text{ k} :}{100 \text{ k} :}$  [V]

The change of output voltage with temperature [mV/ C] is calculated from the following formula. However, the temperature change rates for R<sub>FB1</sub> and R<sub>FB2</sub> are assumed to be the same.

$$\frac{V_{OUT}}{T_a} \text{ [mV/ C]} = 1 + \frac{R_{FB1}}{R_{FB2}} \cdot \frac{V_{OUT}}{T_a} \text{ [ppm/ C]} \cdot 1000$$

(Change of output voltage with temperature) (Set output voltage value) (Output voltage temperature coefficient)







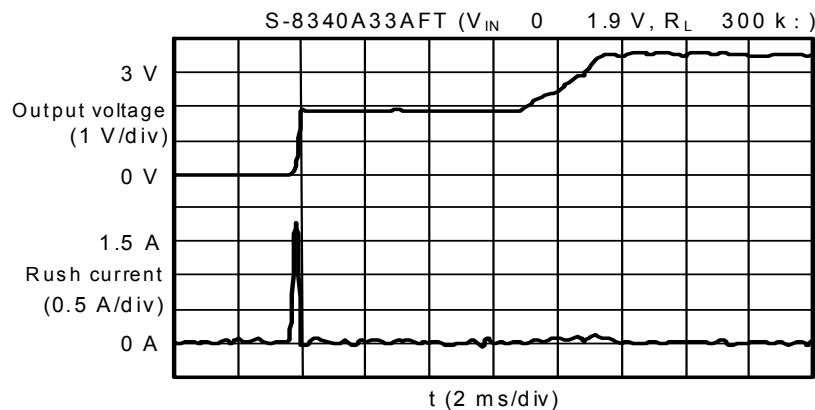
The S-8340 Series is a DC-DC converter using a pulse width modulation method (PWM). In conventional PFM DC-DC converters, pulses are skipped when the output load current is low, causing a fluctuation in the ripple frequency of the output voltage, resulting in an increase in the ripple voltage. The switching frequency does not change, although the pulse width changes from 0 to 82% corresponding to each load current in the S-8340 Series. The ripple voltage generated from switching can thus be eliminated easily through a filter. When the pulse width is 0% (when no load is applied or the input voltage is high), pulses are skipped and the current consumption is low.

The S-8341 Series is a DC-DC converter that automatically switches between a pulse width modulation method (PWM) and a pulse frequency modulation method (PFM) depending on the load current. The S-8341 Series operates under PWM control with the pulse duty changing from 27 to 82% (A and B types) and from 21 to 82% (C and D types) in a high output load current area. The S-8341 Series operates under PFM control with the pulse duty fixed at 27% (A and B types) and at 21% (C and D types) in a low load current area, and pulses are skipped according to the load current. The oscillation circuit thus oscillates intermittently so that the resultant lower self current consumption prevents a reduction in the efficiency at a low load current. The switching point from PWM control to PFM control depends on the external devices (coil, diode, etc.), and input and output voltage values. The S-8341 Series is an especially highly efficient DC-DC converter at an output load current around 1 mA.

The S-8340/8341 Series has a built-in soft-start circuit.

This circuit enables the output voltage ( $V_{OUT}$ ) to rise gradually over the specified soft-start time ( $t_{SS}$ ) to suppress the overshooting of the output voltage and the rush current from the power supply when the power is switched on or the ON/OFF pin is changed to "H".

Generally, a rush current flows to an output capacitor through an inductor and a diode in the step-up circuit immediately after the power is turned on as shown in . Note that the soft-start function of this IC, however, does not limit this current.



The soft-start circuit of the S-8340/8341 Series increases the duty ratio gradually as shown in .  
The soft-start time ( $t_{SS}$ ) can be set with an external capacitor ( $C_{SS}$ ).



If  $f_{OSC}$  600 kHz and  $C_{SS}$  4700 pF, the time until the duty ratio of 50% is reached is 9.7 ms (typ.).

If  $V_{IN}$  2 V, the approximate time until a specific duty ratio is reached is calculated from the following formula :

$$\text{If } f_{OSC} \text{ 600 kHz, } t_{SS} \text{ [ms]} = C_{SS} \text{ [pF]} \frac{8.336 \text{ Duty [\%]} + 682.45}{535000}$$

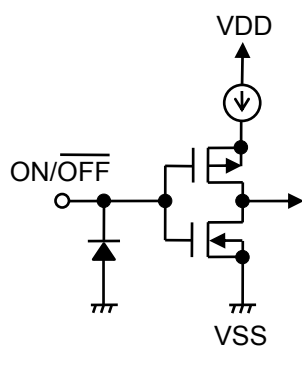
$$\text{If } f_{OSC} \text{ 300 kHz, } t_{SS} \text{ [ms]} = C_{SS} \text{ [pF]} \frac{6.564 \text{ Duty [\%]} + 698}{229000}$$

Even if the IC reaches a certain duty at a duty ratio of 0 to 43%, there may be a delay of the output voltage ( $V_{OUT}$ ) in reaching the specified voltage ( $V_{OUT(S)}$ ). This delay occurs due to the delay of the error amplifier reference voltage in reaching the specified voltage (1.0 V). Note that the maximum delay time may be the value calculated when a duty ratio is 43%.

The  $\overline{\text{ON/OFF}}$  pin stops or starts the step-up operation.

When the  $\overline{\text{ON/OFF}}$  pin is set to "L", all the internal circuits stop operating, reducing power consumption. The EXT pin voltage becomes equal to the  $V_{SS}$  voltage, thereby turning off the switching transistor.

The  $\overline{\text{ON/OFF}}$  pin is configured as shown in and is not either pulled up or pulled down. So, do not use it in a floating state. Applying 0.3 to 0.8 V to the  $\overline{\text{ON/OFF}}$  pin increases current consumption. So do not apply such voltage. When the  $\overline{\text{ON/OFF}}$  pin is not used, connect it to the VDD pin. The  $\overline{\text{ON/OFF}}$  pin does not have hysteresis.



$\overline{\text{ON/OFF}}$ Pin	CR Oscillation Circuit	Output Voltage
"H"	Operating	Set value
"L"	Stopped	# $V_{IN}$

. Voltage obtained by extracting the voltage drop due to DC resistance of the inductor and the diode forward voltage from  $V_{IN}$ .

The current limit circuit of the S-8340/8341 Series protects the external transistors from being damaged by heat due to an overload or magnetic saturation of coils. Inserting a SENSE resistor ( $R_{SENSE}$ ) between the external FET source or external NPN bipolar transistor emitter and  $V_{SS}$  and entering a connection point with a sensor resistor into the SENSE pin enables the current limit to function. Refer to “ ”.

A current limiting comparator in the IC monitors the SENSE pin for reaching the current limit detection voltage ( $V_{SENSE}$  120 mV (typ.)). Upon detection of the voltage, the external transistor is held off for one clock of the oscillator so that the current flowing in the external transistor is limited. At the ON signal of the next clock, the external transistor is turned on and the current limit detection function is resumed.

However, this current limit circuit contains a CR filter with a time constant ( $\tau = 220$  ns (typ.)) between the SENSE pin and the current limiting comparator in the IC to prevent detection errors caused by the spike voltage generated at the SENSE pin. If the time (pulse width  $t_{ON}$  : “H” level time at the EXT pin) after the external transistor turns on until the current limit circuit operates is short, the current value that is actually limited becomes higher than the current limit setting value determined by  $V_{SENSE}/R_{SENSE}$  as a side effect. The actual limit current value ( $I_{LIMIT}$ ) is expressed by the following equation :

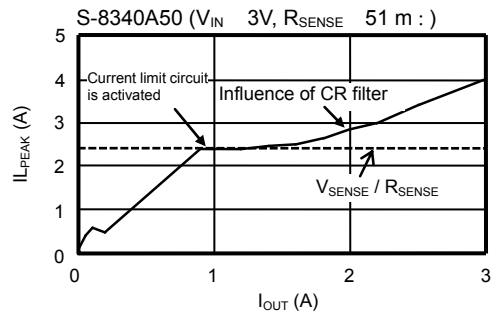
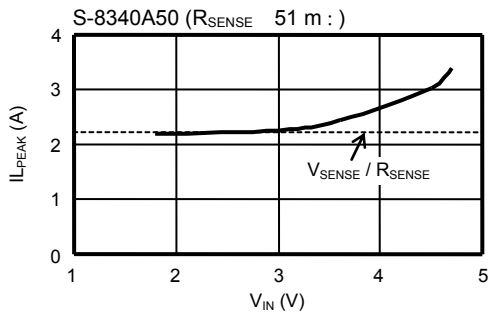
$$I_{LIMIT} = \frac{V_{SENSE}}{R_{SENSE}} \left( 1 - e^{-\frac{t_{ON}}{CR}} \right)$$

CR in the equation is determined by the internal CR filter and varies in the range 116 to 470 ns (220 ns (typ.)).

For example, usage when the current value that the current limit circuit actually functions to raise the current limit set value decided by  $V_{SENSE}/R_{SENSE}$  that includes usage under the conditions that the input voltage become close to the output voltage or situations when the output voltage falls due to the activation of the current limit circuit and become close to the input voltage.

shows an example of the actually measured increase of the peak current flowing through the coil when the current limit circuit functions while the input voltage is nearing the output voltage.

shows an example of the actually measured increase of the peak current flowing through the coil when the output voltage drops and approaches the input voltage by increasing the output current after the current limit circuit functions.



If the current limit circuit is not used, remove  $R_{SENSE}$  and connect the external transistor source or the emitter and the SENSE pin to  $V_{SS}$ .

The S-8340/8341 Series is classified into eight types, according to the control systems (PWM and PWM/PFM switching), oscillation frequencies, and output voltage setting types.

The following describes the features of respective types. Select the type according to the applications.

Two different control systems are available : PWM control system (S-8340 Series) and PWM/PFM switching control system (S-8341 Series).

For applications for which the load current greatly differs between standby and operation, if the efficiency during standby is important, applying the PWM/PFM switching system (S-8341 Series) realizes high efficiency during standby.

For applications for which switching noise is critical, applying the PWM control system (S-8340 Series) whereby switching frequency does not change due to load current allows the ripple voltage to be easily eliminated by using a filter.

Either oscillation frequencies, 600 kHz (A and B types) or 300 kHz (C and D types), can be selected.

The A and B types whereby high operation frequency allows the L value to be reduced, so a small inductor can be used. In addition, use of small output capacitors is effective for downsizing devices.

The C and D types, whereby lower oscillation frequency realizes smaller self-consumption current, are highly efficient under light loads. In particular, the C type, when combined with a PWM/PFM switching control system, drastically improves the operation efficiency when the output load current is approximately 1 mA.

Either fixed output type (A and C types) or external setting type (B and D types) can be selected.

The A and C types, whereby output voltage can be internally set between 2.5 and 6.0 V in the 0.1 V steps, realizes highly accurate output voltage of  $\pm 2.0\%$  with internal highly resistant and highly accurate resistors.

In the B and D types, the output voltage can be adjusted in the range 2.5 to 6.0 V by adding external resistors ( $R_{FB1}$  and  $R_{FB2}$ ) and a capacitor ( $C_{FB}$ ).

A temperature gradient can be provided by installing a thermistor in series to  $R_{FB1}$  and  $R_{FB2}$ .

The resistance of  $R_{FB1}$  and  $R_{FB2}$  must not exceed 2 M $\Omega$ , and set the ratio of  $R_{FB1}$  to  $R_{FB2}$  so that the FB pin is at 1.0 V.

Add  $C_{FB}$  in parallel with  $R_{FB1}$  to prevent unstable operation due to output oscillation.

Set  $C_{FB}$  so that  $f_{OSC} = 1/(2\pi \cdot C_{FB} \cdot R_{FB1})$  is 0.1 to 20 kHz (normally, 10 kHz).

Example :  $V_{OUT} = 3.0$  V,  $R_{FB1} = 200$  k $\Omega$ ,  $R_{FB2} = 100$  k $\Omega$ ,  $C_{FB} = 100$  pF

The accuracy of the output voltage  $V_{OUT}$  set with resistors  $R_{FB1}$  and  $R_{FB2}$  is affected by the absolute precision of external resistors  $R_{FB1}$  and  $R_{FB2}$ , the FB pin input current ( $I_{FB}$ ) and IC power supply voltage ( $V_{DD}$ ) as well as the precision of the voltage at FB pin ( $\pm 2.0\%$ ).

When it is assumed that  $I_{FB}$  is 0 nA, the maximum absolute value variations of external resistors  $R_{FB1}$  and  $R_{FB2}$  are  $R_{FB1,max.}$  and  $R_{FB2,max.}$ , the minimum absolute value variations of external resistors  $R_{FB1}$  and  $R_{FB2}$  are  $R_{FB1,min.}$  and  $R_{FB2,min.}$ , and the shift of the output voltage due to the dependence of voltage on  $V_{DD}$  is  $\Delta V$ , the minimum value ( $V_{OUT,min.}$ ) and maximum value ( $V_{OUT,max.}$ ) of variations of  $V_{OUT}$  are expressed by the following formulas :

$$V_{OUT \text{ min.}} = \left(1 \frac{R_{FB1 \text{ min.}}}{R_{FB2 \text{ max.}}}\right) 0.98 \text{ V} \approx$$

$$V_{OUT \text{ max.}} = \left(1 \frac{R_{FB1 \text{ max.}}}{R_{FB2 \text{ min.}}}\right) 102 \text{ V} \approx$$

$R_{FB1}$  and  $R_{FB2}$  must be adjusted in order to set the voltage accuracy of  $V_{OUT}$  to the IC output voltage accuracy ( $V_{OUT}$  2.0 %) or lower. The smaller  $R_{FB1}$  and  $R_{FB2}$  are, the less  $V_{OUT}$  is affected by the absolute value accuracy of  $R_{FB1}$  and  $R_{FB2}$ . The smaller  $R_{FB1}$  and  $R_{FB2}$  are, the less  $V_{OUT}$  is affected by  $I_{FB}$ .

To reduce the influence due to  $I_{FB}$  that affects variations of  $V_{OUT}$ , the  $R_{FB2}$  value must be set to a value sufficiently lower than the input impedance at the FB pin (1 V/50 nA 20 M : (max.)).

Reactive current flows through  $R_{FB1}$  and  $R_{FB2}$ . Unless the reactive current value is limited as low as possible with respect to the actual load current, efficiency decreases. Therefore,  $R_{FB1}$  and  $R_{FB2}$  should be sufficiently large.

:

Since the accuracy of  $V_{OUT}$  and reactive current must be traded off, they must be considered according to application requirements.

The table below provides a rough guide for selecting a product type according to the application requirements of the application.

Choose the product that gives you the largest number of circles (O).

	S-8340				S-8341			
	A	B	C	D	A	B	C	D
The set output voltage is 6 V or less	☆		☆		☆		☆	
Set an output voltage freely		☆		☆		☆		☆
The efficiency under light loads (approx. 1mA) is an important factor					{	{	~	~
To be operated with a medium load current (200 mA class)	{	{	{	{	{	{	{	{
To be operated with a high load current (1 A class)	{	{	{	{	{	{	{	{
It is important to have a low-ripple voltage	{	{			{	{		
Downsizing of external components is important	~	~			~	~		

The symbol "☆" denotes an indispensable condition, while the symbol "{" indicates that the corresponding series has superiority in that aspect. The symbol "~" indicates particularly high superiority.

The inductance value (L value) greatly affects the maximum output current ( $I_{OUT}$ ) and the efficiency ( ).

As the L value is reduced gradually, the peak current ( $I_{PK}$ ) increases and  $I_{OUT}$  increases. As the L value is made even smaller,  $I_{OUT}$  decreases since the efficiency degrades and the current driveability is insufficient.

As the L value is increased, the dissipation in the switching transistor due to  $I_{PK}$  decreases, and the efficiency reaches the maximum at a certain L value. As the L value is made even larger, the efficiency degrades since the dissipation due to the series resistance of the inductor increases.  $I_{OUT}$  also decreases.

In the S-8340/8341 Series, as the L value is increased, the output voltage may be unstable depending on the conditions of the input voltage, output voltage, and load current. Select the L value after performing a thorough valuation under actual use conditions. The guidelines for the L range are from 2.2 to 22 H for the A and B types, and 4.7 to 47 H for the C and D types.

The recommended L value is 5 to 10 H for the A and B types, and 10 to 22 H for the C and D types.

When choosing an inductor, attention to its allowable current should be paid since the current exceeding the allowable value will cause magnetic saturation in the inductor, leading to a marked decline in efficiency and a breakdown of the IC due to large current.

An inductor should therefore be selected so that  $I_{PK}$  does not surpass its allowable current.  $I_{PK}$  is represented by the following equations in non-continuous operation mode.

$$I_{PK} = \sqrt{\frac{2 I_{OUT} (V_{OUT} - V_F - V_{IN})}{f_{OSC} L}}$$

Where  $f_{OSC}$  is the oscillation frequency, L is the inductance value of the inductor, and  $V_F$  is the forward voltage of the diode.  $V_F$  should be appropriately 0.4 V.

For example, if a power supply with the input voltage ( $V_{IN}$ ) 3 V, output voltage ( $V_{OUT}$ ) 5 V, and load current ( $I_{OUT}$ ) 30 mA is used,  $f_{OSC}$  600 kHz when the S-8340A50AFT is used. When 10 H is selected for the L value,  $I_{PK}$  155 mA from the above formula. Therefore, in this case, an inductor with a permissible current of 155 mA or higher for the L value of 10 H should be selected.

Use an external diode that meets the following requirements :

- yLow forward voltage (Schottky barrier diode is recommended.)
- yHigh switching speed (50 ns max.)
- yThe reverse-direction withstand voltage is  $V_{OUT} - V_F$  or higher.
- yThe current rating is  $I_{PK}$  or larger.

A capacitor inserted on the input side ( $C_{IN}$ ) improves the efficiency by reducing the power impedance and stabilizing the input current. Select a  $C_{IN}$  value according to the impedance of the power supply used. Approximately 47 to 100 F is recommended for a capacitance depending on the impedance of the power source and load current value. For the output side capacitor ( $C_L$ ), select a large capacitance with low ESR (Equivalent Series Resistance) for smoothing the ripple voltage. When the input voltage is extremely high or the load current is extremely large, the output voltage may become unstable. In this case the unstable area will become narrow by selecting a large capacitance for an output capacitor. A tantalum electrolyte capacitor is recommended since the unstable area widens when a capacitor with a large ESR, such as an aluminum electrolyte capacitor, or a capacitor with a small ESR, such as a ceramic capacitor, is chosen.

It is recommended that a capacitor of which the capacitance is 47 to 200 F and ESR is 40 to 270 m : be selected. Fully evaluate input and output capacitors under actual operating conditions, then select them.

Enhancement (N-channel) MOS FET type or bipolar (NPN) type can be used for the external transistors.

The EXT pin can directly drive an N-channel MOS FET. When an N-channel MOS FET is used, efficiency will be 2 to 3% higher than that achieved by an NPN bipolar transistor since the MOS FET switching speed is faster and power dissipation due to the base current is avoided.

A large current may flow at power on with some MOS FETs selected. Perform thorough evaluation using the actual devices to select. The recommended gate capacitance of the MOS FET to be used is 1200 pF or smaller.

The important parameters in selecting a MOS FET are threshold voltage, breakdown voltage between drain and source, total gate capacitance, on-resistance, and the current rating.

The EXT pin voltage swings between  $V_{DD}$  and  $V_{SS}$ . If  $V_{DD}$  is low, a MOS FET of which the threshold voltage is low enough so that the MOS FET is completely turned on must be used. If  $V_{DD}$  is high, the breakdown voltage between the gate and source must be higher by at least several volts.

During the step-up operation, voltage  $V_{OUT} + V_F$  is applied between the drain and source of the MOS FET. So the breakdown voltage between the drain and source should be higher than the  $V_{OUT} + V_F$  voltage by at least several volts.

The total gate capacitance and the on-resistance affect the efficiency.

The larger the total gate capacitance becomes and the higher the input voltage becomes, the more the power dissipation for charging and discharging the gate capacitance by switching operation increases, and affects the efficiency at low load current region. If the efficiency at low load is important, select MOS FETs with a small total gate capacitance.

In the regions where the load current is high, the efficiency is affected by power dissipation caused by the resistance of the MOS FETs. If the efficiency under heavy load is particularly important in the application, choose MOS FETs which have an on-resistance as low as possible. As for the current rating, select a MOS FET whose maximum continuous drain current rating is higher than  $I_{PK}$ .

and in “ show sample circuit diagrams using Sanyo Electric Co., Ltd. 2SD1628G for the bipolar transistor (NPN). The driveability for increasing the output current by means of a bipolar transistor depend on the  $h_{FE}$  and  $R_b$  values of that bipolar transistor.

The  $R_b$  value is given by the following equation :

$$R_b = \frac{V_{DD} - 0.7}{I_b} - \frac{0.4}{|I_{EXTH}|}$$

Find the necessary base current ( $I_b$ ) using the  $h_{FE}$  value of the bipolar transistor by the equation,  $I_b = I_{PK}/h_{FE}$ , and select a smaller  $R_b$  value.

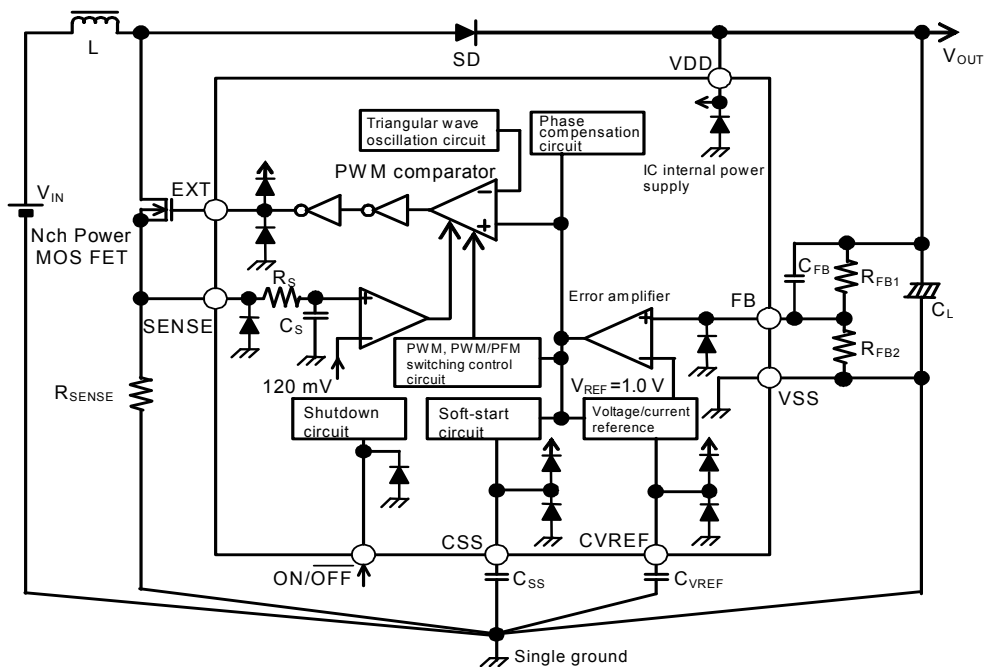
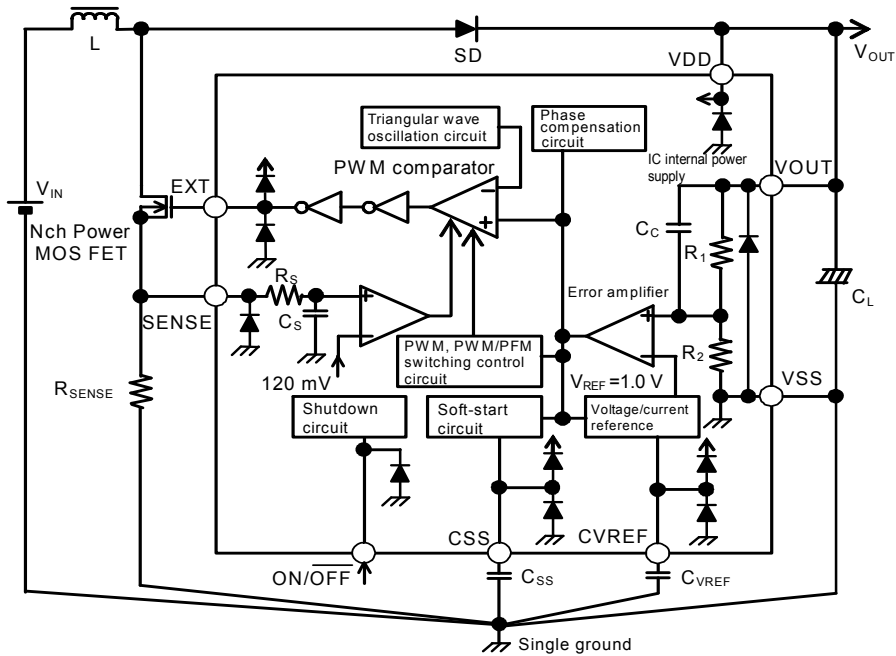
A small  $R_b$  value can increase the output current, but the efficiency decreases. A current may flow as the pulses or voltage drops take place due to the wiring resistance or some other reason. Determine an optimum value through experimentation.

In addition, if a speed-up capacitor ( $C_b$ ) is inserted in parallel with the resistance ( $R_b$ ) as shown in and , the switching loss will be reduced, leading to a higher efficiency.

Select a  $C_b$  value by using the following equation as a guide :

$$C_b = \frac{1}{2 R_b f_{osc} - 0.1}$$

However, the optimum  $C_b$  value differs depending upon the characteristics of the bipolar transistor. Select a  $C_b$  value after performing a thorough evaluation.

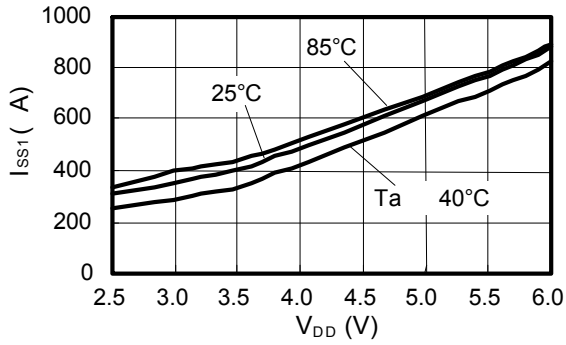




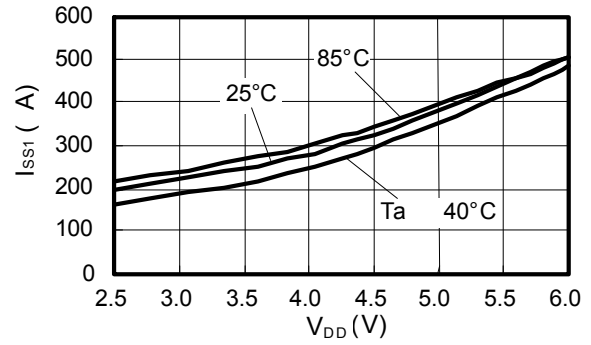


- y Mount the external capacitors, diode, coil, and other peripheral parts as close to the IC as possible, and make a one-point grounding.
- y Characteristic ripple voltage and spike noise occur in IC containing switching regulators. Moreover rush current flows at the time of a power supply injection. Because these largely depend on the coil, the capacitor and impedance of power supply used, fully check them using an actually mounted model.
- y Make sure that dissipation of the switching transistor especially at high temperature will not surpass the power dissipation of the package.
- y To stabilize operation, use a capacitor with a low ESR as a bypass capacitor between the VDD and VSS pins of the IC, and install and wire it with a short distance and a low impedance. Connect  $C_{VREF}$  to the VSS pin.
- y The main circuit of the IC operates on the internal power supply connected to the CVREF pin.  $C_{VREF}$  is a bypass capacitor that stabilizes the internal power supply. Use a 0.01 to 1 F ceramic capacitor as  $C_{VREF}$  and install and wire it to assure a short distance and a low impedance.
- y Switching regulator performance varies depending on the design of PC patterns, peripheral circuits and parts. Thoroughly evaluate the actual device when setting. When using parts other than those which are recommended, contact the ABLIC Inc. marketing department.
- y Do not apply an electrostatic discharge to this IC that exceeds the performance ratings of the built-in electrostatic protection circuit.
- y ABLIC Inc. claims no responsibility for any disputes arising out of or in connection with any infringement by products including this IC of patents owned by a third party.

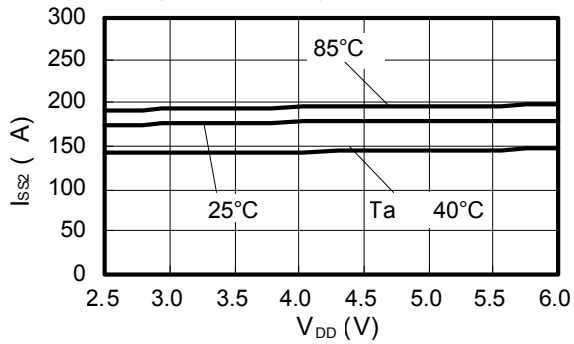
S-8340A33A (f<sub>OSC</sub> : 600 kHz)



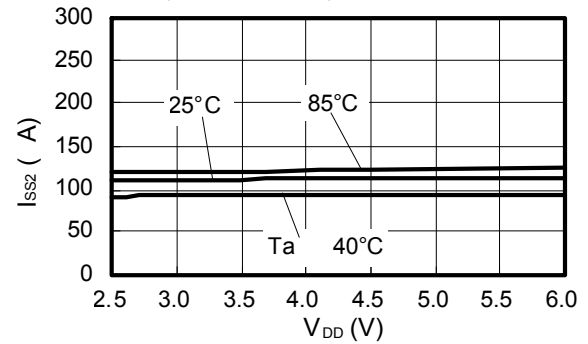
S-8340C33A (f<sub>OSC</sub> : 300 kHz)



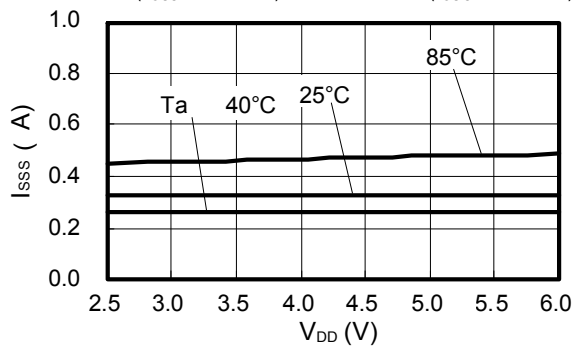
S-8340A33A (f<sub>OSC</sub> : 600 kHz)



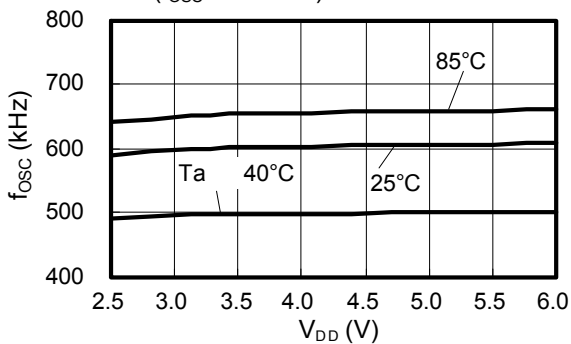
S-8340C33A (f<sub>OSC</sub> : 300 kHz)



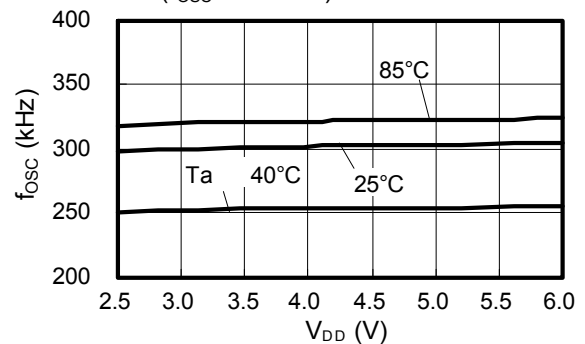
S-8340A33A (f<sub>OSC</sub> : 600 kHz) / S-8340C33A (f<sub>OSC</sub> : 300 kHz)



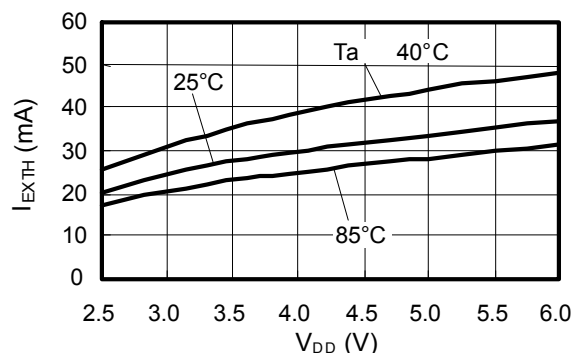
S-8340A33A (f<sub>OSC</sub> : 600 kHz)



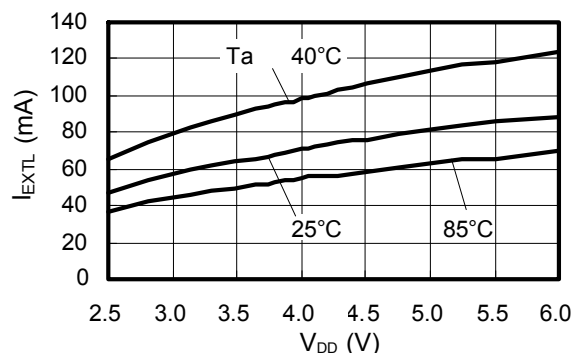
S-8340C33A (f<sub>OSC</sub> : 300 kHz)



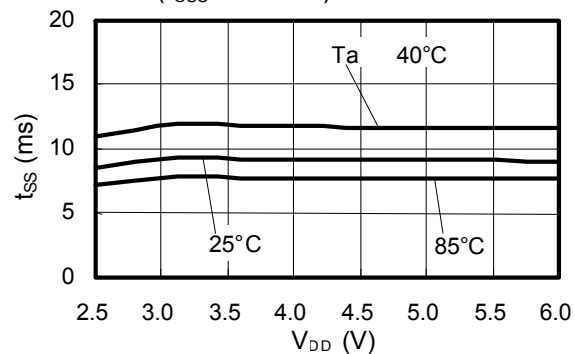
S-8340A33A (f<sub>OSC</sub> : 600 kHz) / S-8340C33A (f<sub>OSC</sub> : 300 kHz)



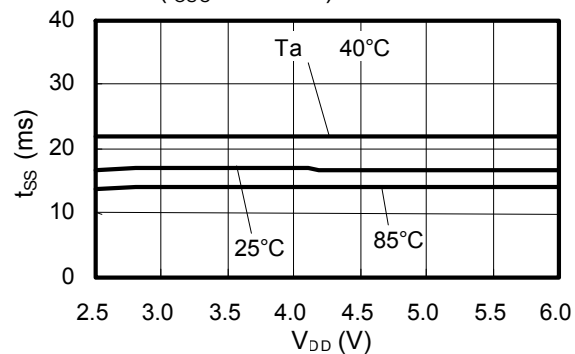
S-8340A33A (f<sub>OSC</sub> : 600 kHz) / S-8340C33A (f<sub>OSC</sub> : 300 kHz)



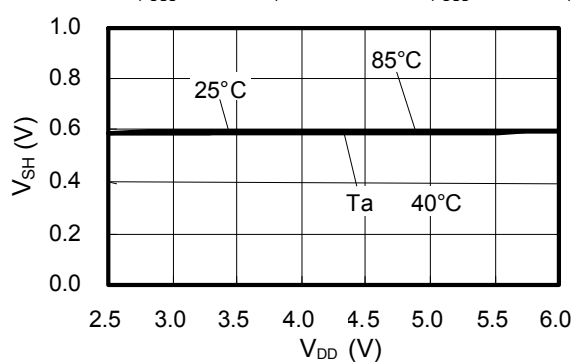
S-8340A33A (f<sub>OSC</sub> : 600 kHz)



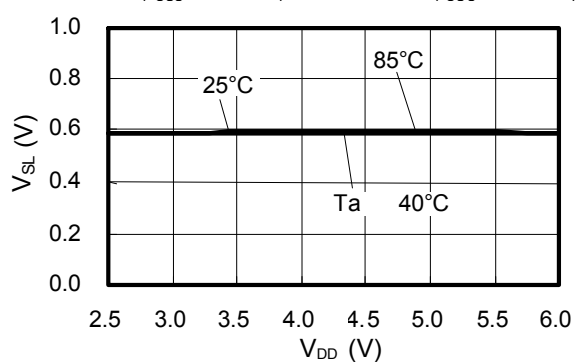
S-8340C33A (f<sub>OSC</sub> : 300 kHz)



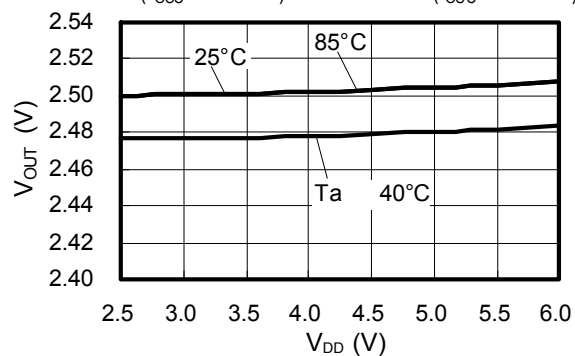
S-8340A33A (f<sub>OSC</sub> : 600 kHz) / S-8340C33A (f<sub>OSC</sub> : 300 kHz)



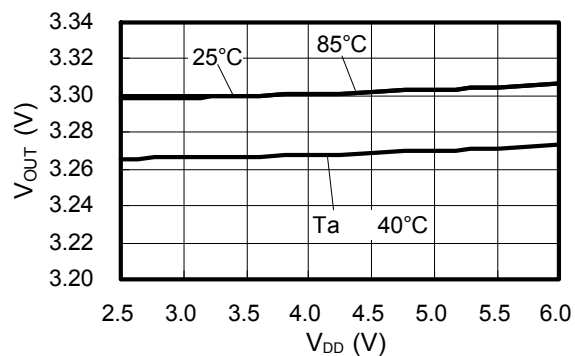
S-8340A33A (f<sub>OSC</sub> : 600 kHz) / S-8340C33A (f<sub>OSC</sub> : 300 kHz)



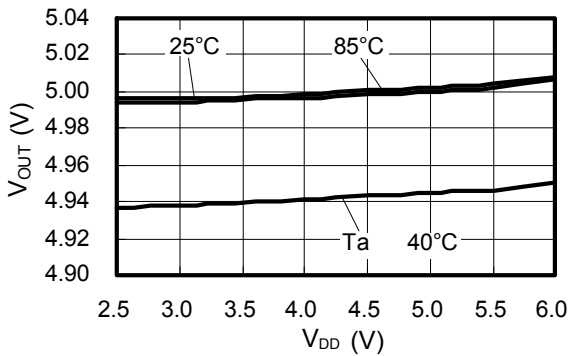
S-8340A25A (f<sub>OSC</sub> : 600 kHz) / S-8340C25A (f<sub>OSC</sub> : 300 kHz)



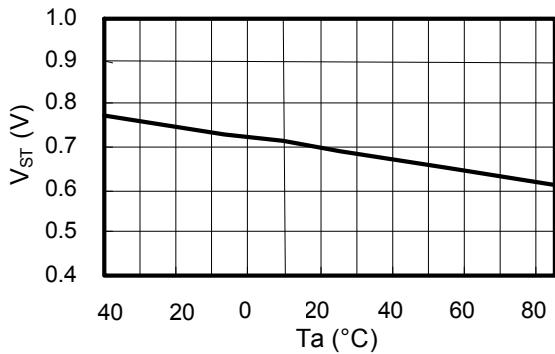
S-8340A33A (f<sub>OSC</sub> : 600 kHz) / S-8340C33A (f<sub>OSC</sub> : 300 kHz)



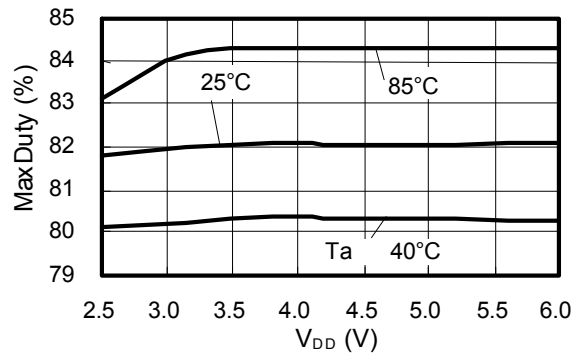
S-8340A50A (f<sub>osc</sub> : 600 kHz) / S-8340C50A (f<sub>osc</sub> : 300 kHz)



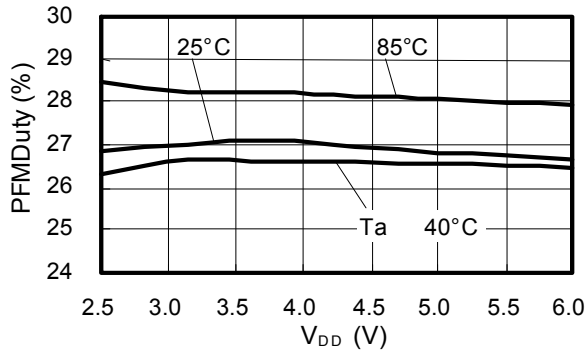
S-8340A33A (f<sub>osc</sub> : 600 kHz) / S-8340C33A (f<sub>osc</sub> : 300 kHz)



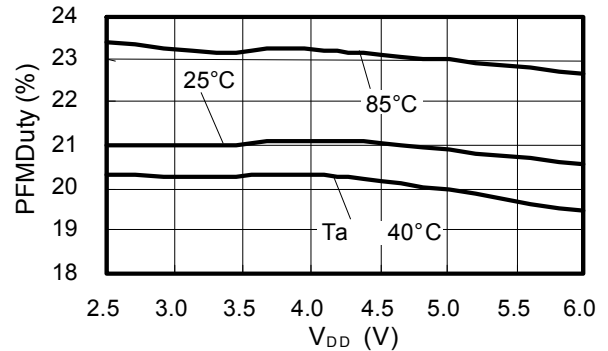
S-8340A33A (f<sub>osc</sub> : 600 kHz) / S-8340C33A (f<sub>osc</sub> : 300 kHz)



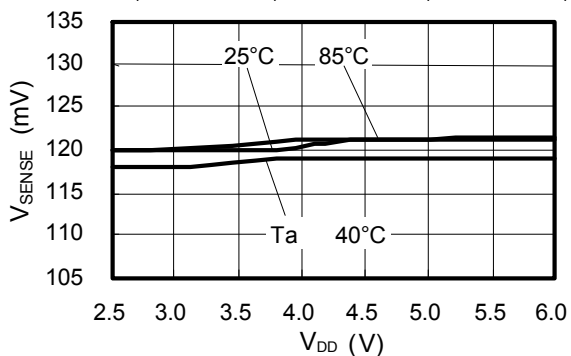
S-8341A33A (f<sub>osc</sub> : 600 kHz)

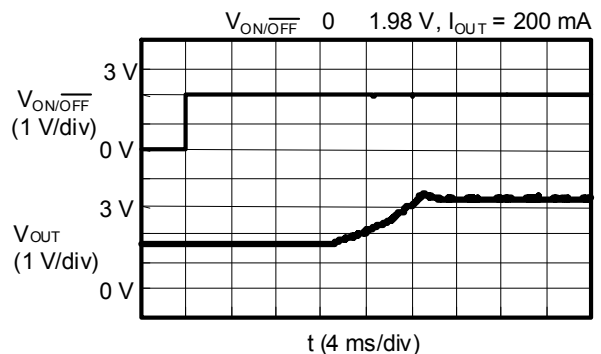
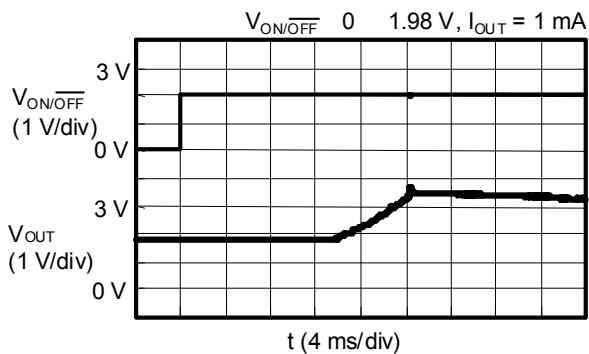
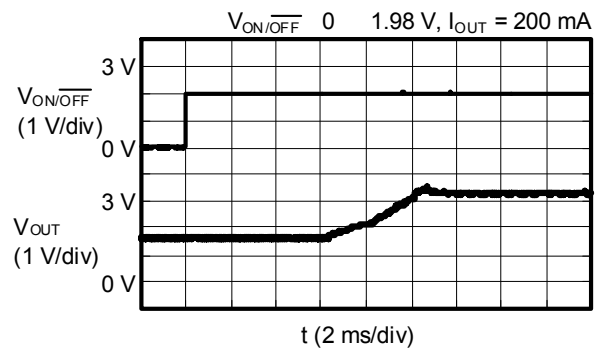
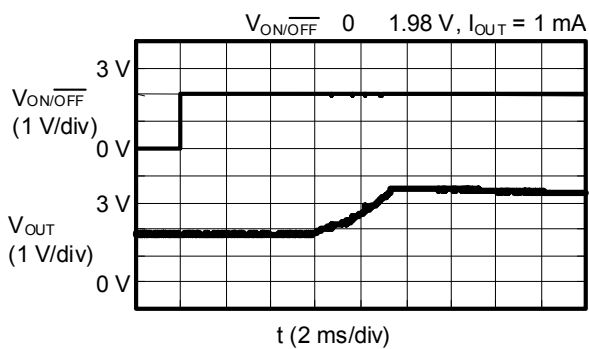
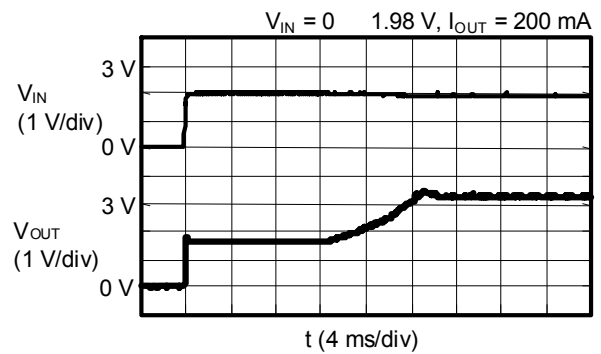
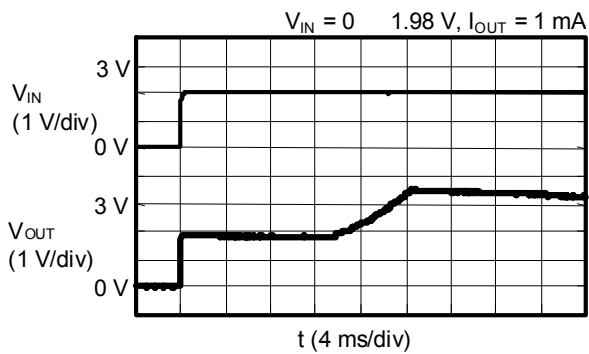
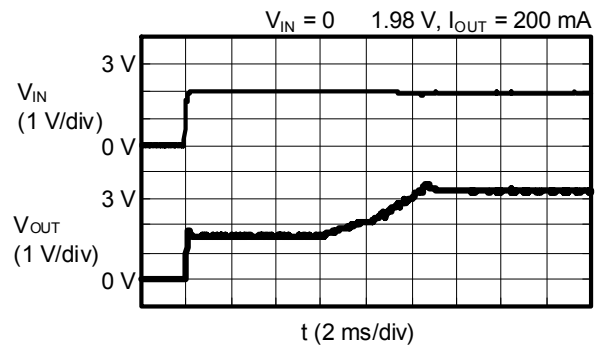
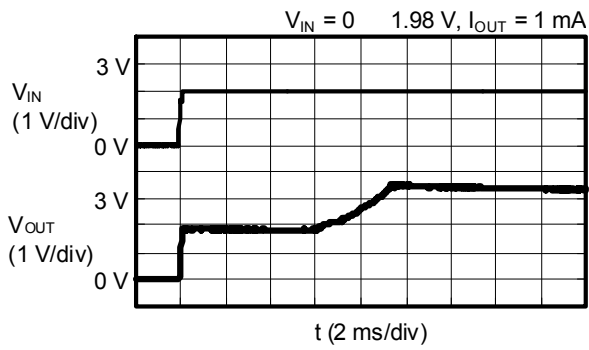


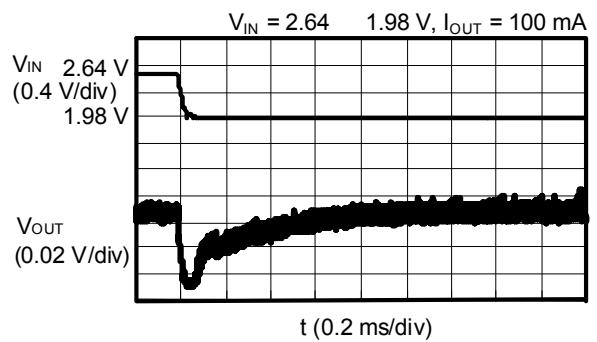
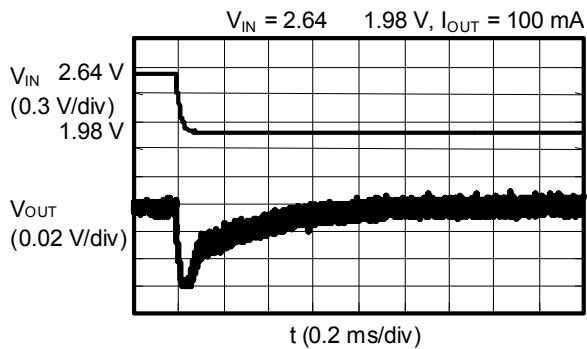
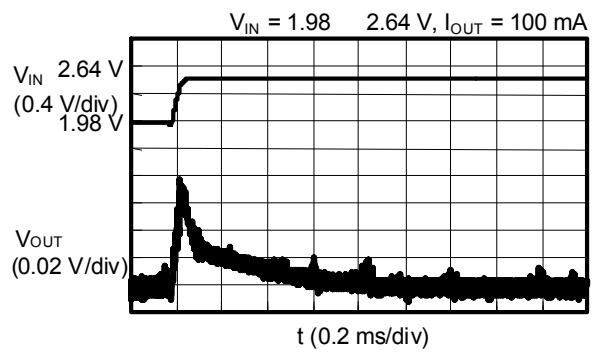
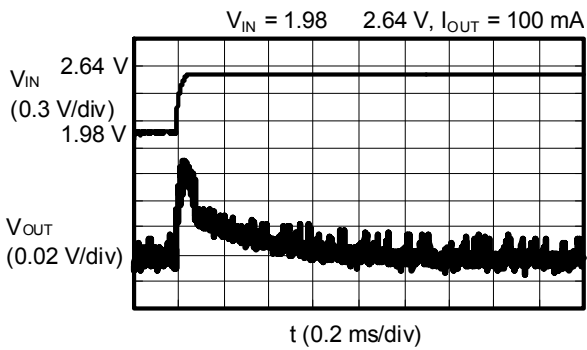
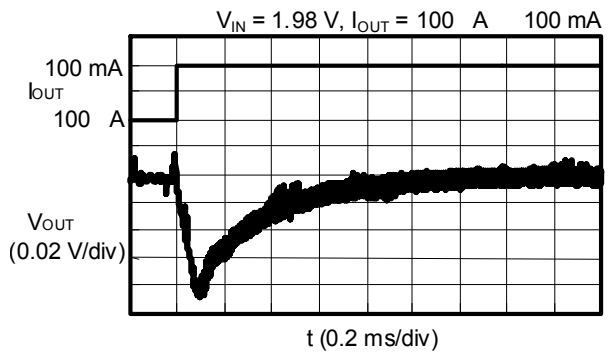
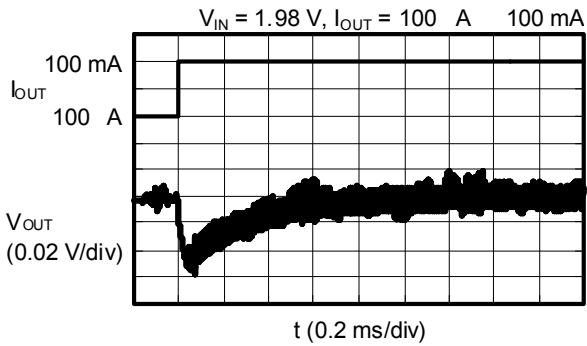
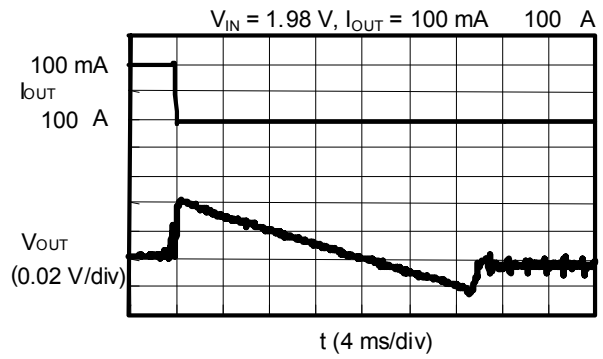
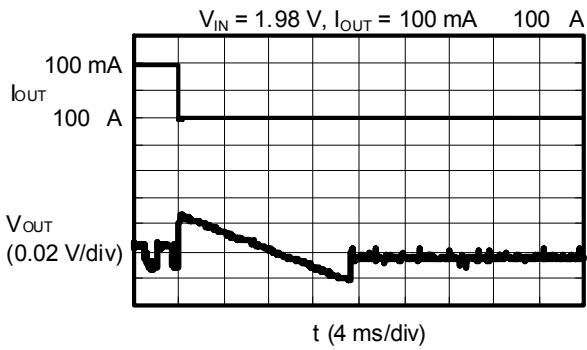
S-8341C33A (f<sub>osc</sub> : 300 kHz)



S-8340A33A (f<sub>osc</sub> : 600 kHz) / S-8340C33A (f<sub>osc</sub> : 300 kHz)











No.	Product Name	Output Voltage	Inductor	Transistor	Diode	Output Capacitor	Sense Resistor	Application
(25)	S-8341A25AFT	2.5 V	CDRH5D18/4.1 H	NDS335N	RB491D	F920J476MB3 1	0 :	
(26)			CDRH124/10 H	FTS2001	RBO81L-20	F951C476MG1 2		
(27)	S-8341A33AFT	3.3 V	CDRH5D18/4.1 H	NDS335N	RB491D	F920J476MB3 1		
(28)			CDRH124/10 H	FTS2001	RBO81L-20	F951C476MG1 2		
(29)	S-8341A50AFT	5.0 V	CDRH5D18/4.1 H	NDS335N	RB491D	F951A476MF1 1		
(30)			CDRH124/10 H	FTS2001	RBO81L-20	F951C476MG1 2		

CDRH5D18 + NDS335N + RB491D: For small and thin parts of which height is 2 mm or shorter (The maximum current of an external part should be set to 1.7 A.)

CDRH124 + FTS2001 + RBO81L-20: For heavy load current (The maximum current of an external part should be set to 4.5 A.)

No.	Product Name	Output Voltage	Inductor	Transistor	Diode	Output Capacitor	Sense Resistor	Application
(31)	S-8341C25AFT	2.5 V	CDRH6D28/10 H	FDN335N	RB491D	F951C476MG1 1	0 :	
(32)			CDRH124/10 H	FTS2001	RBO81L-20	F951C476MG1 2		
(33)	S-8341C33AFT	3.3 V	CDRH6D28/10 H	FDN335N	RB491D	F951C476MG1 1		
(34)			CDRH124/10 H	FTS2001	RBO81L-20	F951C476MG1 2		
(35)	S-8341C50AFT	5.0 V	CDRH6D28/10 H	FDN335N	RB491D	F951C476MG1 1		
(36)			CDRH124/10 H	FTS2001	RBO81L-20	F951C476MG1 2		

CDRH6D28 + FDN335N + RB491D: For part heights of 3 mm and high efficiency

CDRH124 + FTS2001 + RBO81L-20: For optimizing the load current driveability

No.	Product Name	Output Voltage	Inductor	Transistor	Diode	Output Capacitor	Sense Resistor	Application
(37)	S-8340A25AFT	2.5 V	CDRH5D18/4.1 H	NDS335N	RB491D	F920J476MB3 1 F920J476MB3 2	0 :	
(38)			CDRH124/10 H	FTS2001	RBO81L-20	F951C476MG1 2 F951A107MG1 2		
(39)	S-8341A25AFT		CDRH5D18/4.1 H	NDS335N	RB491D	F920J476MB3 1 F920J476MB3 2		
(40)			CDRH124/10 H	FTS2001	RBO81L-20	F951C476MG1 2 F951A107MG1 2		
(41)	S-8340A33AFT	3.3 V	CDRH5D18/4.1 H	NDS335N	RB491D	F920J476MB3 1 F920J476MB3 2		
(42)			CDRH124/10 H	FTS2001	RBO81L-20	F951C476MG1 2 F951A107MG1 2		
(43)	S-8341A33AFT		CDRH5D18/4.1 H	NDS335N	RB491D	F920J476MB3 1 F920J476MB3 2		
(44)			CDRH124/10 H	FTS2001	RBO81L-20	F951C476MG1 2 F951A107MG1 2		
(45)	S-8340A50AFT	5.0 V	CDRH5D18/4.1 H	NDS335N	RB491D	F951A476MF1 1 F951A476MF1 2		
(46)			CDRH124/10 H	FTS2001	RBO81L-20	F951C476MG1 2 F951A107MG1 2		
(47)	S-8341A50AFT		CDRH5D18/4.1 H	NDS335N	RB491D	F951A476MF1 1 F951A476MF1 2		
(48)			CDRH124/10 H	FTS2001	RBO81L-20	F951C476MG1 2 F951A107MG1 2		

CDRH5D18 + NDS335N + RB491D: For small and thin parts of which the height is 2 mm or shorter (The maximum current of an external part should be set to 1.7 A.)

CDRH124 + FTS2001 + RBO81L-20: For heavy load current (The maximum current of an external part should be set to 4.5 A.)

No.	Product Name	Output Voltage	Inductor	Transistor	Diode	Output Capacitor	Sense Resistor	Application
(49)	S-8340C25AFT	2.5 V	CDRH6D28/10 H	FDN335N	RB491D	F951C476MG1 1 F951C476MG1 2	0 :	
(50)			CDRH124/10 H	FTS2001	RBO81L-20	F951C476MG1 2 F951A107MG1 2		
(51)	S-8341C25AFT		CDRH6D28/10 H	FDN335N	RB491D	F951C476MG1 1 F951C476MG1 2		
(52)			CDRH124/10 H	FTS2001	RBO81L-20	F951C476MG1 2 F951A107MG1 2		
(53)	S-8340C33AFT	3.3 V	CDRH6D28/10 H	FDN335N	RB491D	F951C476MG1 1 F951C476MG1 2		
(54)			CDRH124/10 H	FTS2001	RBO81L-20	F951C476MG1 2 F951A107MG1 2		
(55)	S-8341C33AFT		CDRH6D28/10 H	FDN335N	RB491D	F951C476MG1 1 F951C476MG1 2		
(56)			CDRH124/10 H	FTS2001	RBO81L-20	F951C476MG1 2 F951A107MG1 2		
(57)	S-8340C50AFT	5.0 V	CDRH6D28/10 H	FDN335N	RB491D	F951C476MG1 1 F951C476MG1 2		
(58)			CDRH124/10 H	FTS2001	RBO81L-20	F951C476MG1 2 F951A107MG1 2		
(59)	S-8341C50AFT		CDRH6D28/10 H	FDN335N	RB491D	F951C476MG1 1 F951C476MG1 2		
(60)			CDRH124/10 H	FTS2001	RBO81L-20	F951C476MG1 2 F951A107MG1 2		

CDRH6D28 + FDN335N + RB491D: For part heights of 3 mm and high efficiency

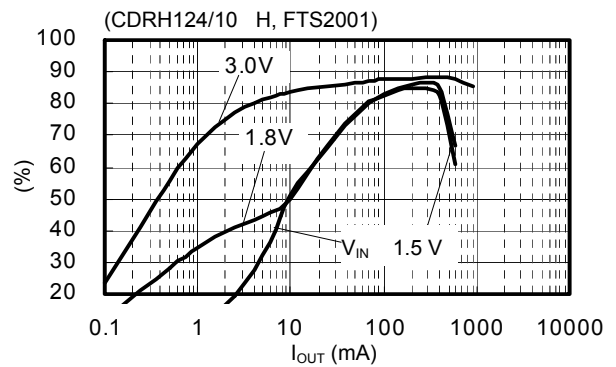
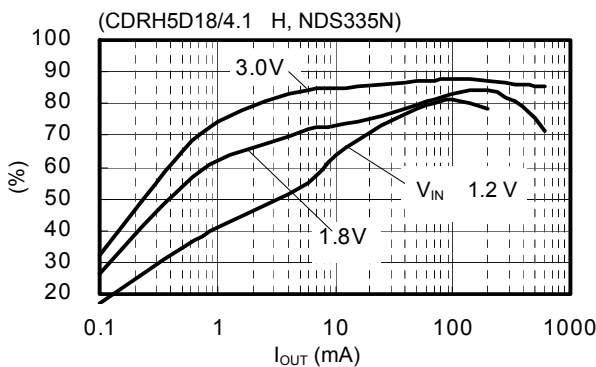
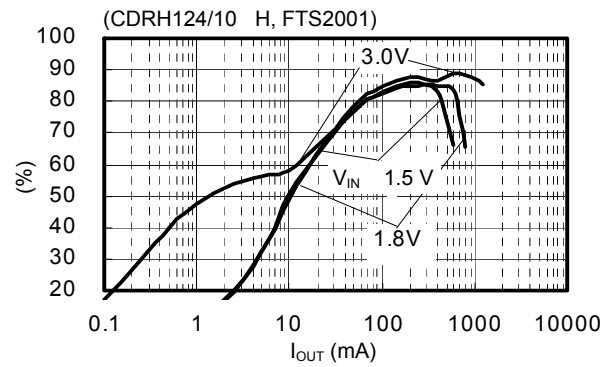
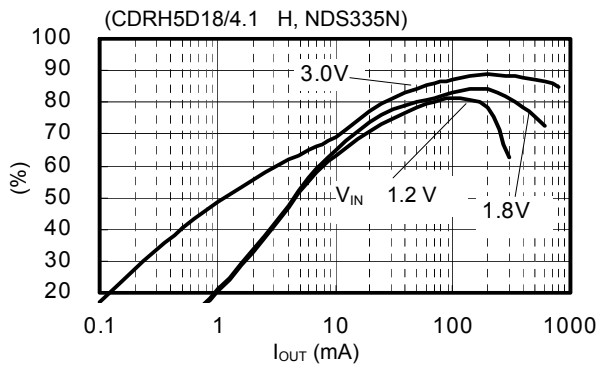
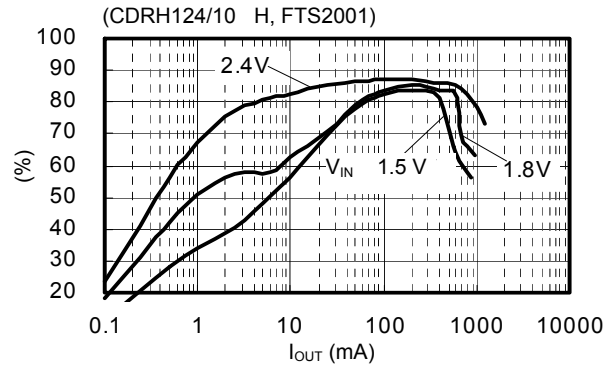
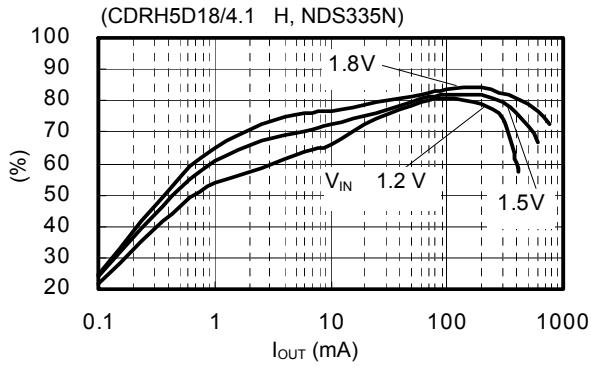
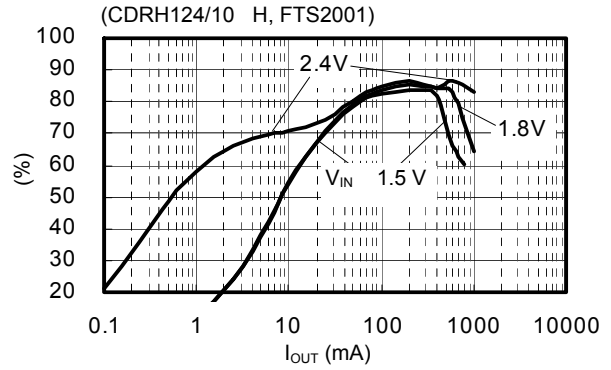
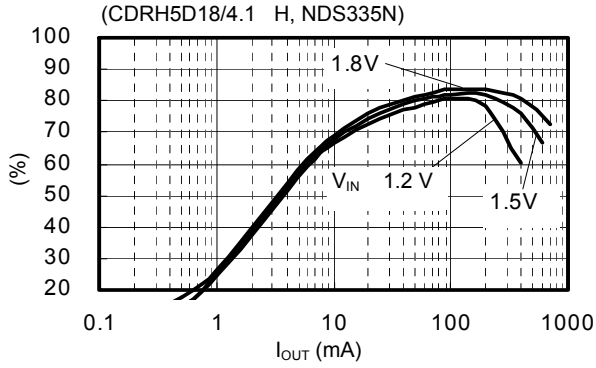
CDRH124 + FTS2001 + RBO81L-20: For optimizing the load current driveability

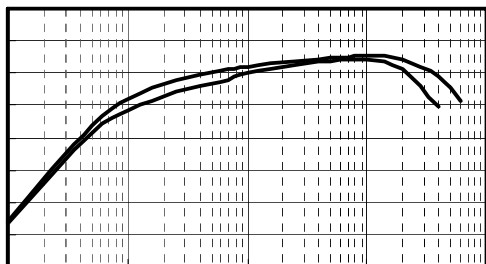
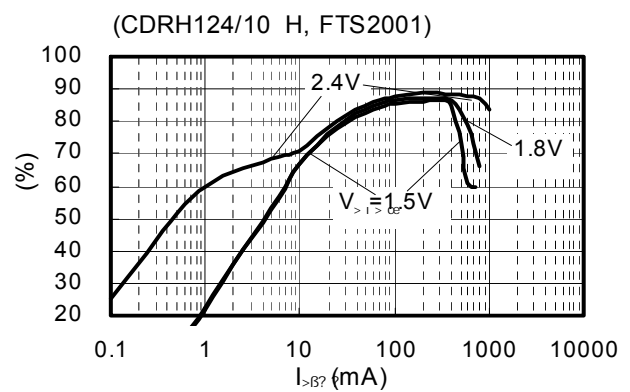
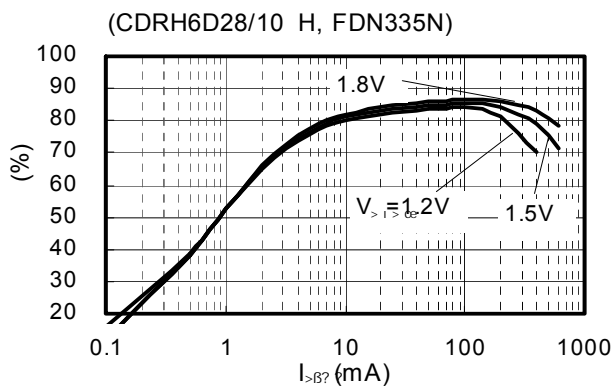
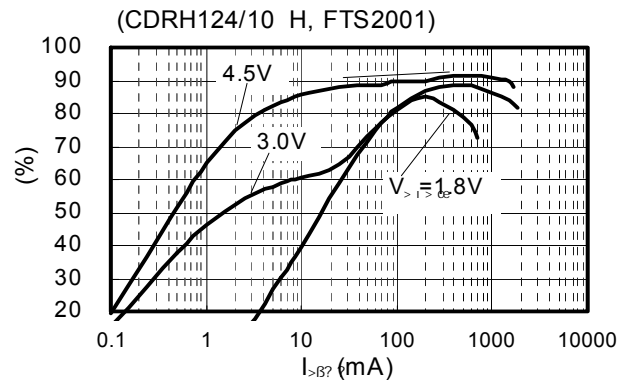
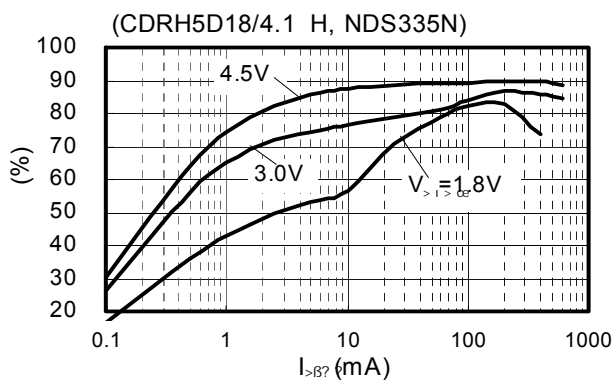
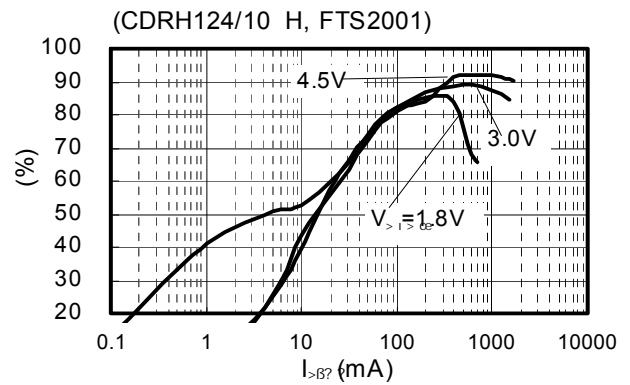
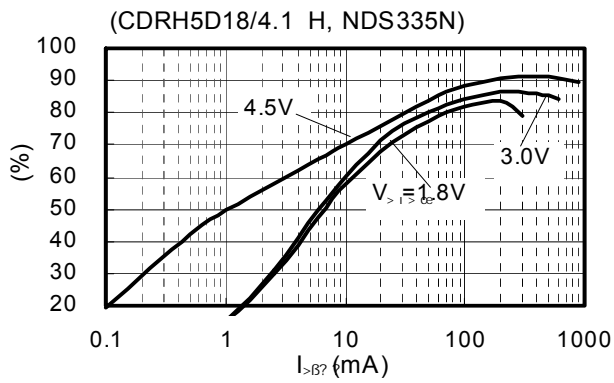
The following shows the performance of external parts.

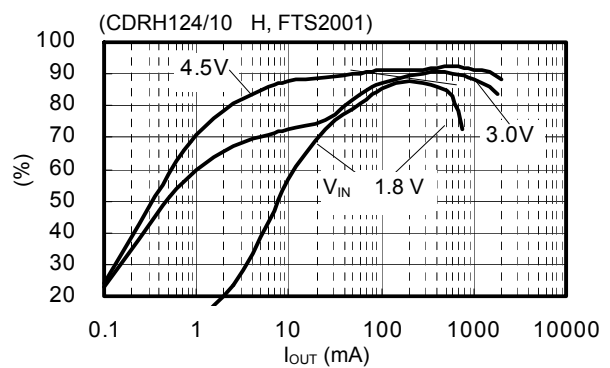
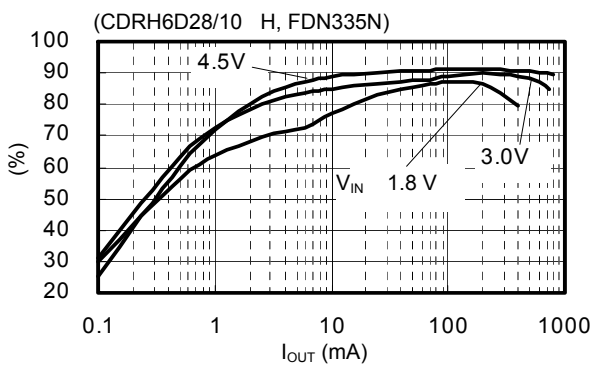
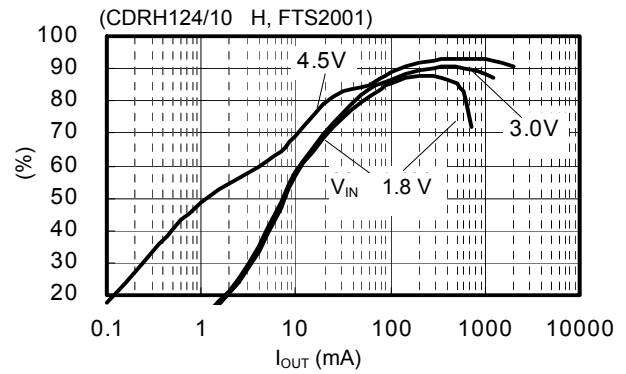
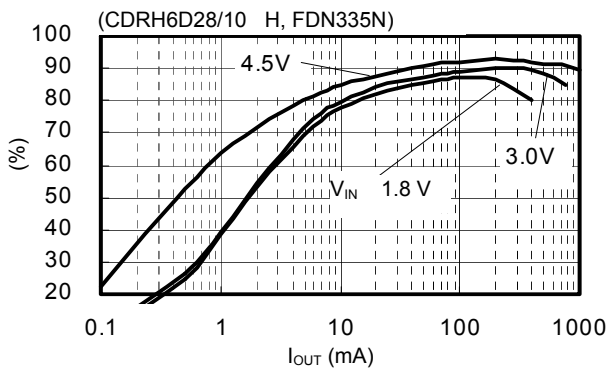
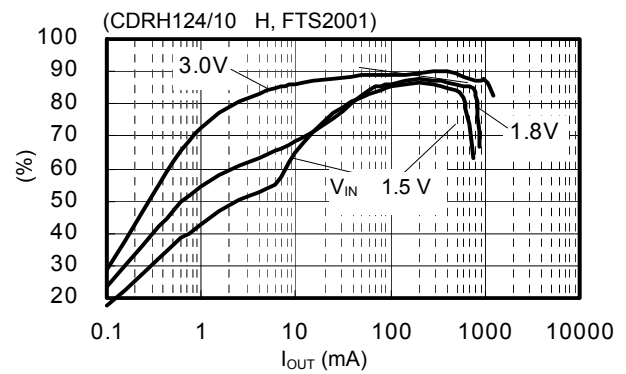
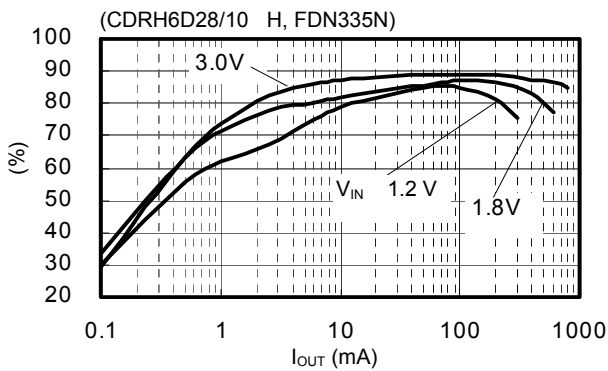
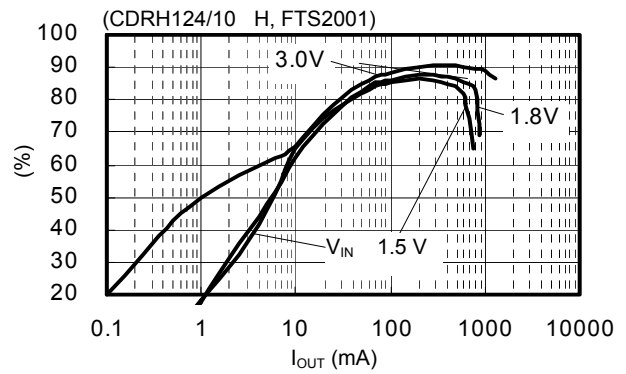
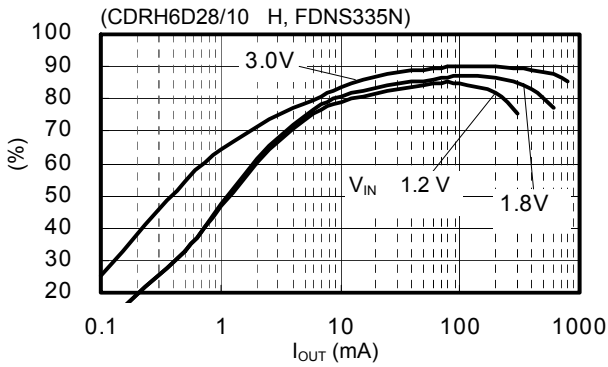
Component	Product Name	Manufacturer	Performance				
			L	DC resistance	Max. Current	Diameter	Height
Inductor	CDRH5D18	Sumida Corporation	4.1 H	0.042 : typ. 0.057 : max.	1.95 A	5.7 mm typ. 6.0 mm max.	1.8 mm typ. 2.0 mm max.
	CDRH124		10 H	0.028 : max.	4.5 A	12.0 mm typ. 12.3 mm max.	4.5 mm max.
	CDRH6D28		10 H	0.048 : typ. 0.065 : max.	1.70 A	6.7 mm typ. 7.0 mm max.	3.0 mm max.
Diode	RB491D	Rohm Corporation	Forward current 1.0 A @ $V_F = 0.45$ V, $V_{rm} = 25$ V				
	RB081L 20		Forward current 5.0 A @ $V_F = 0.45$ V, $V_{rm} = 25$ V				
Capacitor (output capacitance) (tantalum electrolytic capacitor)	F951C476MG1	Nichicon Corporation	47 F, 16 V, 5.5 4.8 2.3 mm max., ESR = 0.08 : (nominal value)				
	F951A476MF1		47 F, 10 V, 5.5 4.8 2.0 mm max., ESR = 0.1 : (nominal value)				
	F920J476MB3		47 F, 6.3 V, 3.6 3 1.2 mm max., ESR = 0.27 : (nominal value)				
	F951A107MG1		100 F, 10 V, 5.5 4.8 2.3 mm max., ESR = 0.08 : (nominal value)				
External transistor (N-channel FET)	NDS335N	Fairchild Semiconductor Corporation	$V_{DSS} = 20$ V max., $V_{GSS} = 8$ V max., $I_D = 1.7$ A max., $V_{th} = 0.5$ V to 1 V, $C_{iss} = 240$ pF typ., $R_{DS(ON)} = 0.14$ : max. ( $V_{GS} = 2.7$ V), SOT-23-3 package or equivalent				
	FDN335N		$V_{DSS} = 20$ V max., $V_{GSS} = 8$ V max., $I_D = 1.7$ A max., $V_{th} = 0.4$ V to 1.5 V, $C_{iss} = 310$ pF typ., $R_{DS(ON)} = 0.10$ : max. ( $V_{GS} = 2.5$ V), SOT-23-3 package or equivalent				
	FTS2001	Sanyo Electric Co., Ltd.	$V_{DSS} = 20$ V max., $V_{GSS} = 8$ V max., $I_D = 5$ A max., $V_{th} = 0.4$ V to 1.3 V, $C_{iss} = 750$ pF typ., $R_{DS(ON)} = 0.046$ : max. ( $V_{GS} = 2.5$ V), 8-Pin TSSOP package				

The manufacturer recommends the FDN335N as an alternative for the NDS335N.

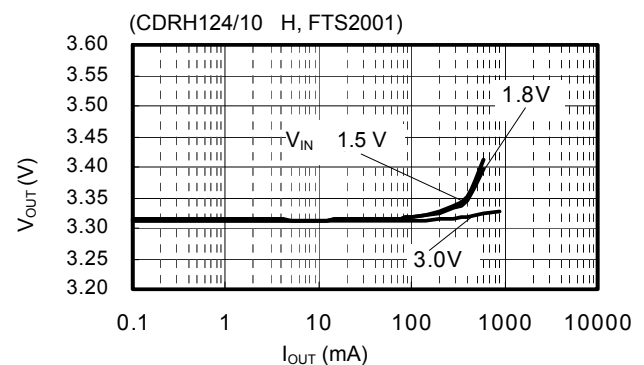
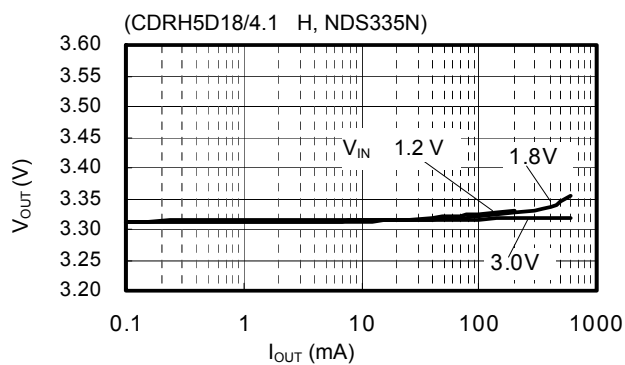
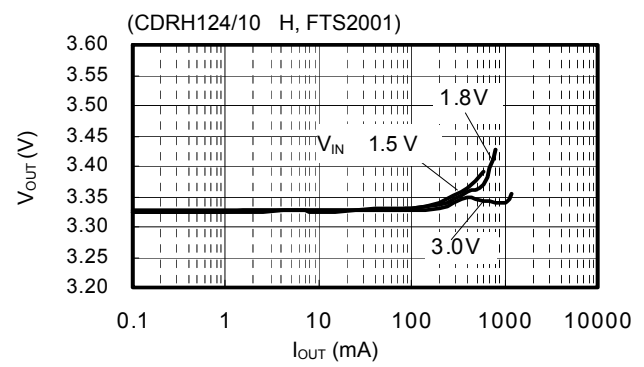
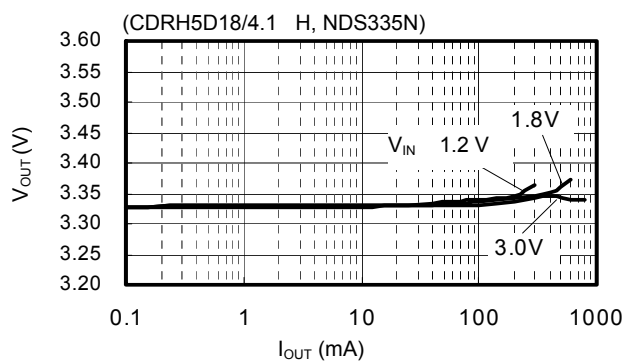
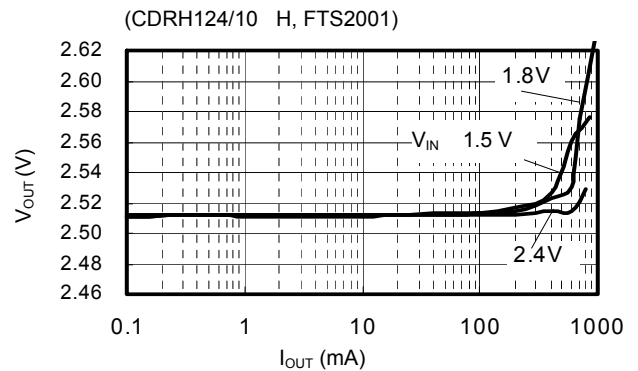
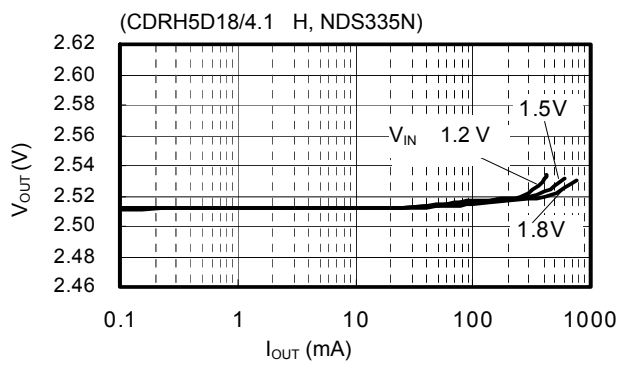
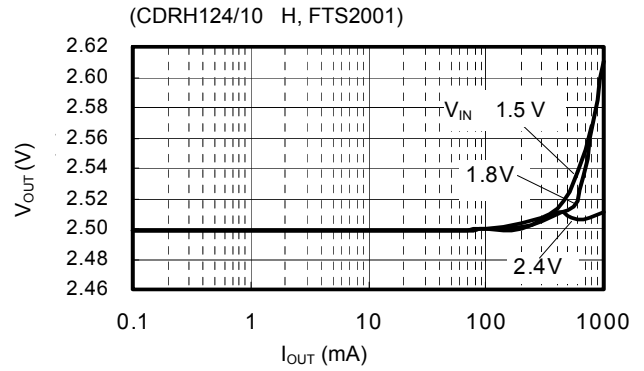
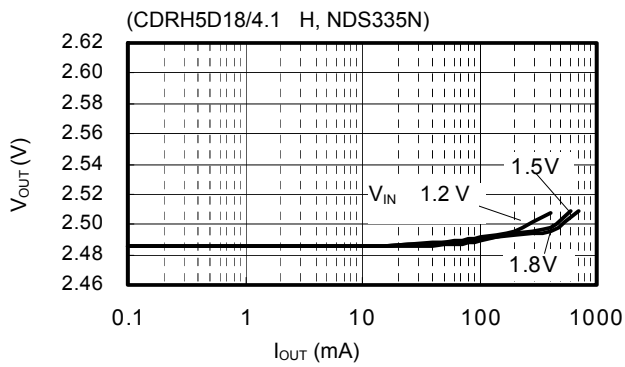
The following shows the actual output current ( $I_{OUT}$ ) vs. efficiency (%) characteristics when the S-8340/8341 Series is used under conditions (1) to (24) in and .



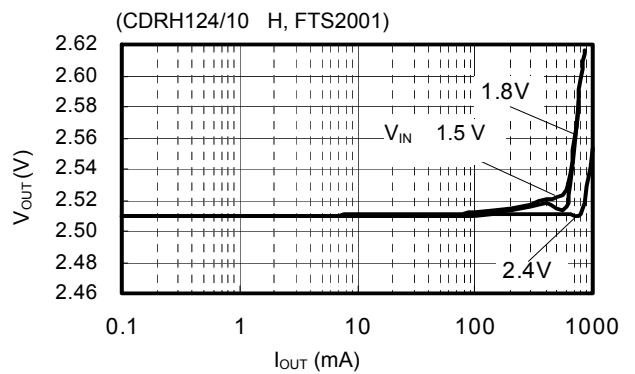
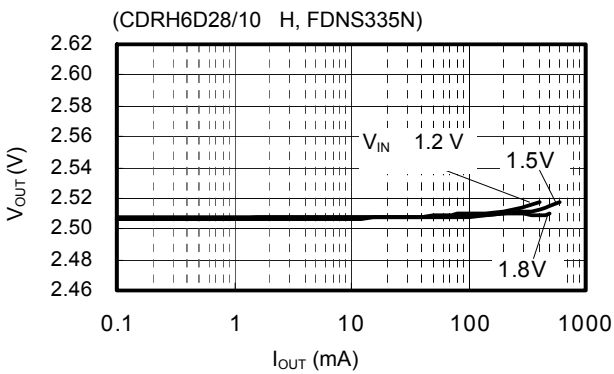
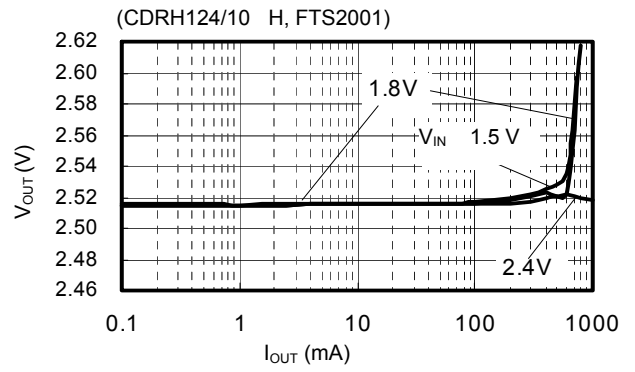
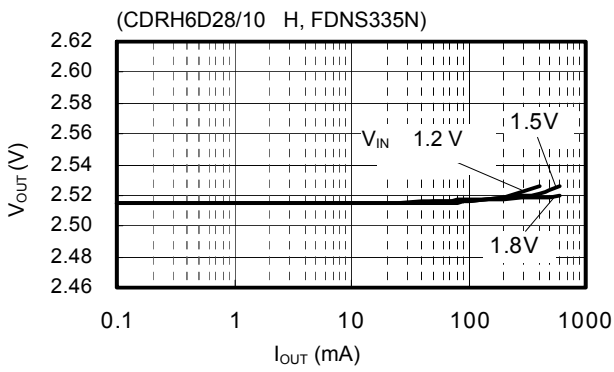
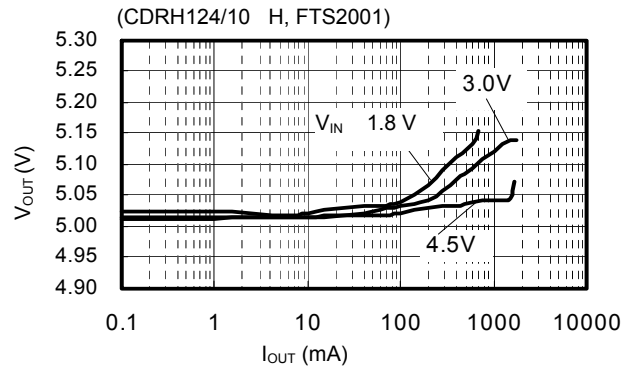
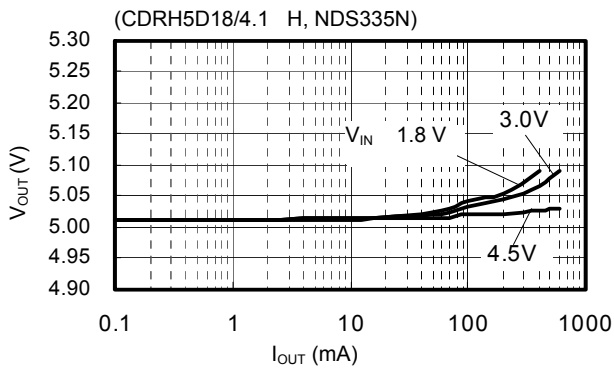
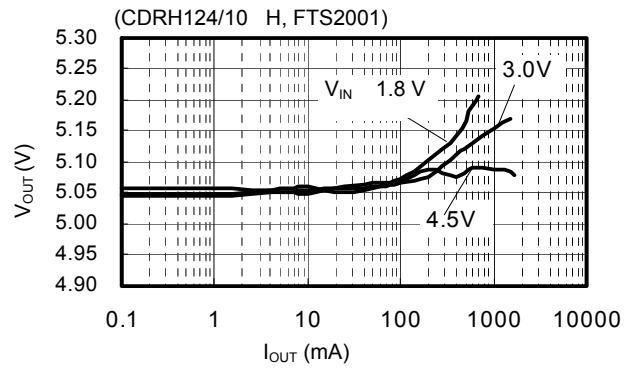
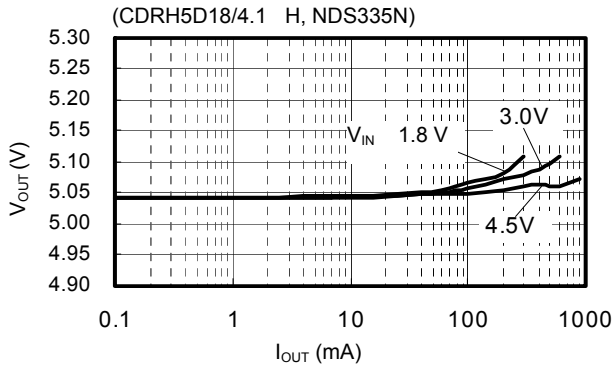


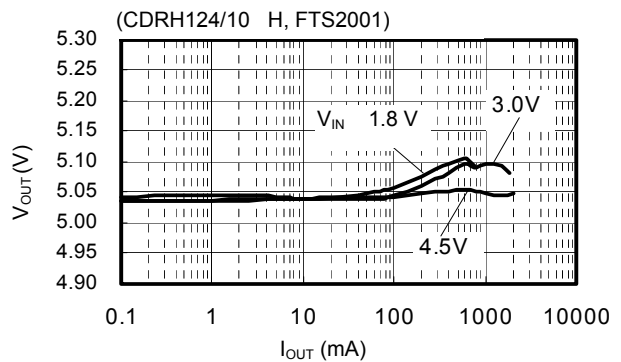
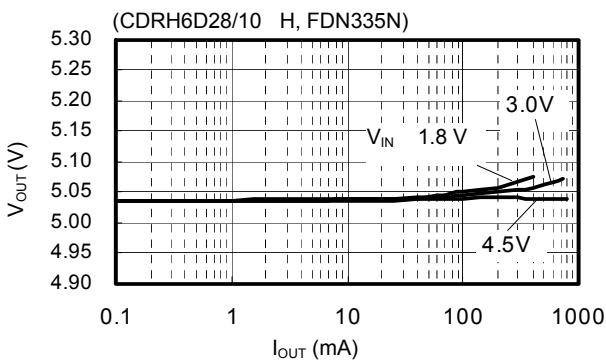
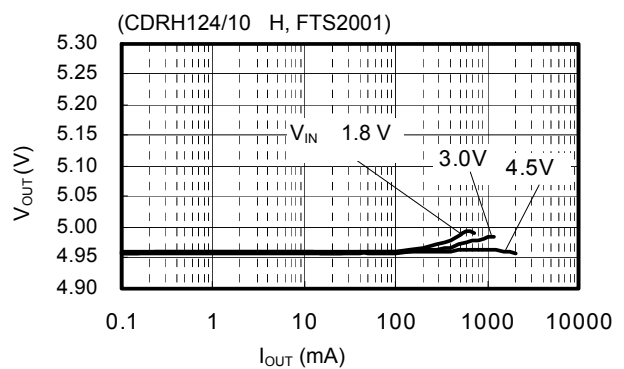
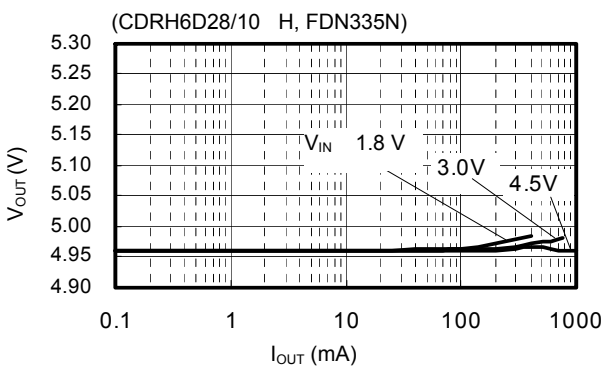
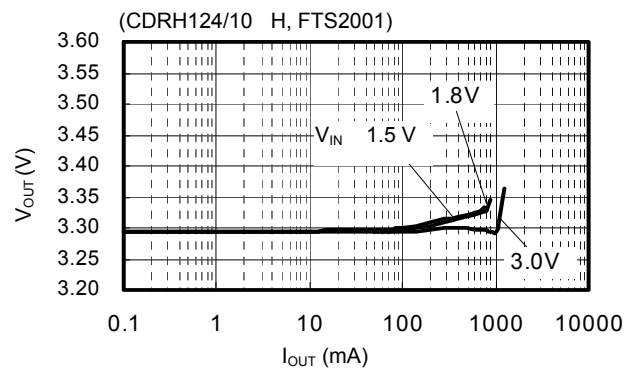
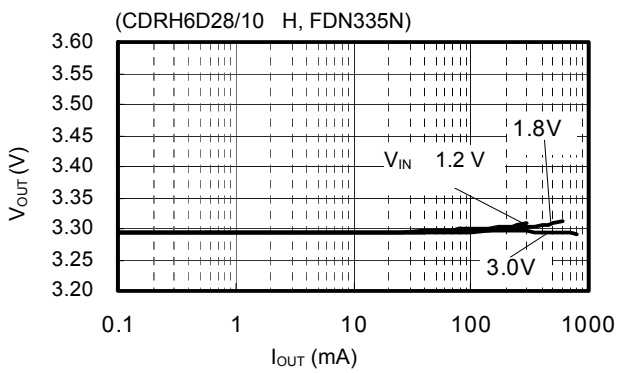
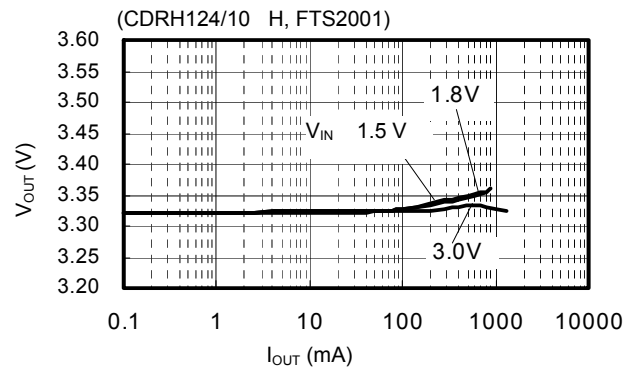
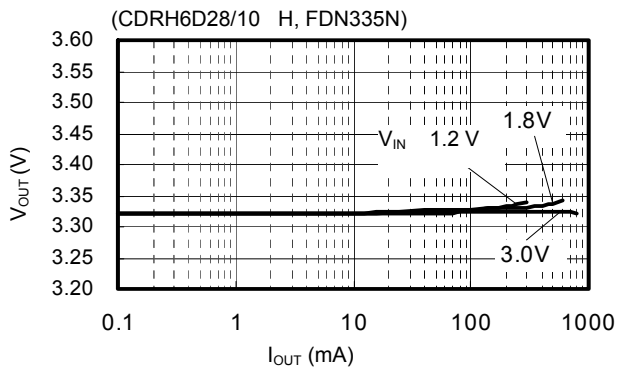


The following shows the actual output current ( $I_{OUT}$ ) vs. output voltage ( $V_{OUT}$ ) characteristics when the S-8340/8341 Series is used under conditions (1) to (24) in and .

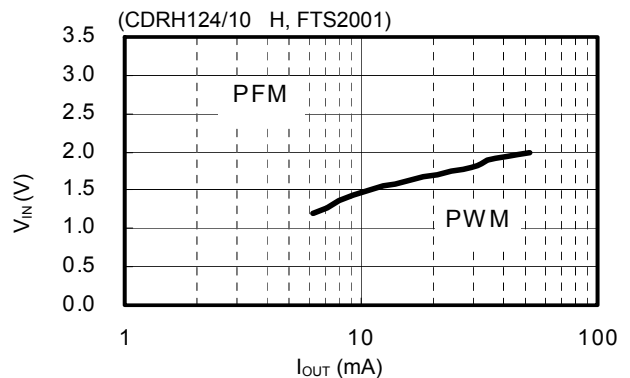
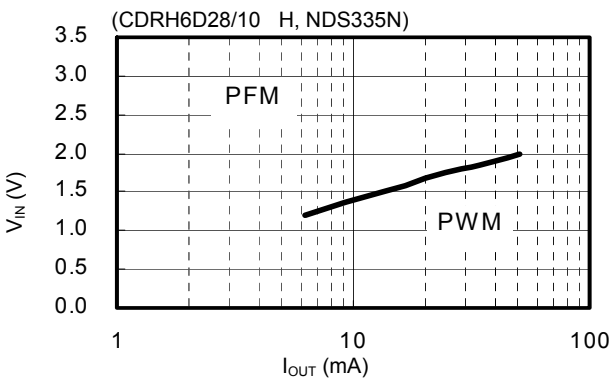
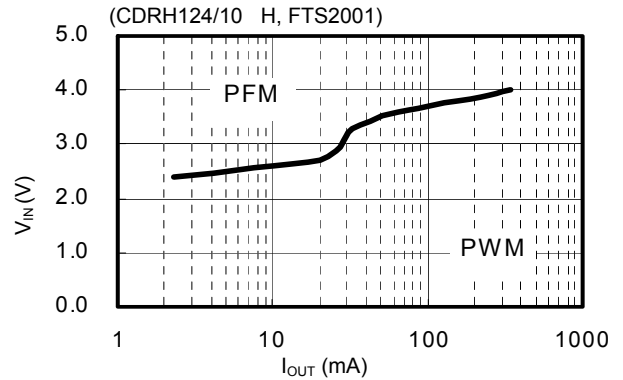
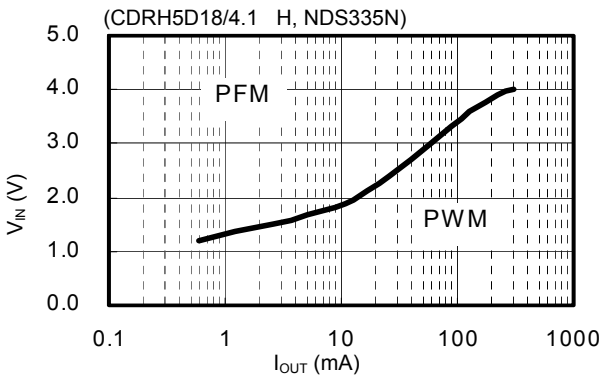
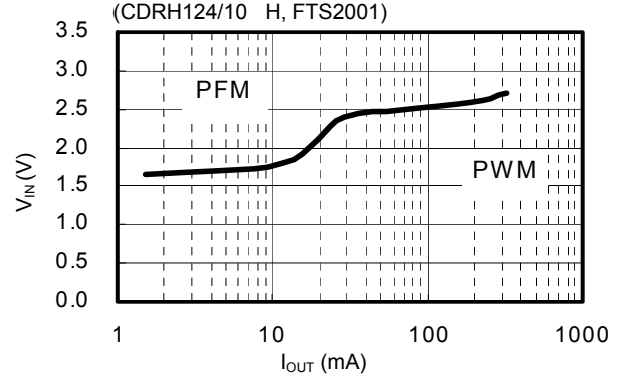
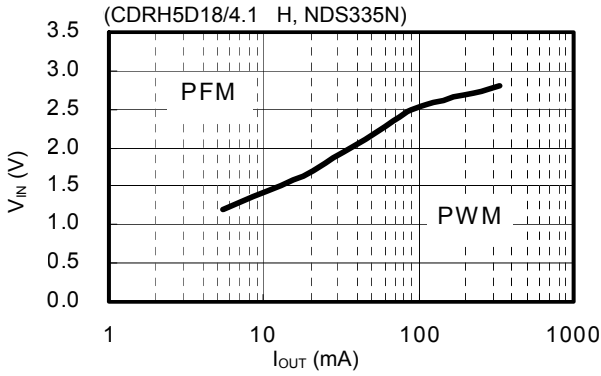
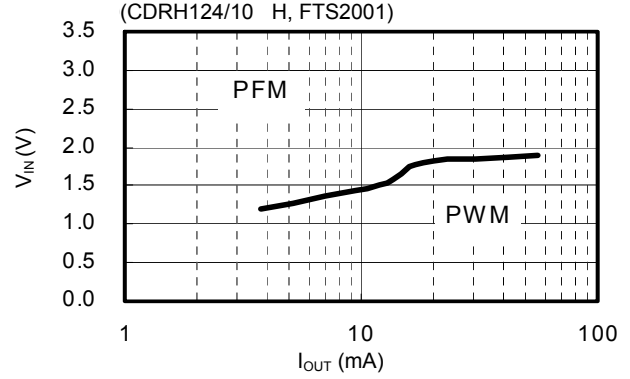
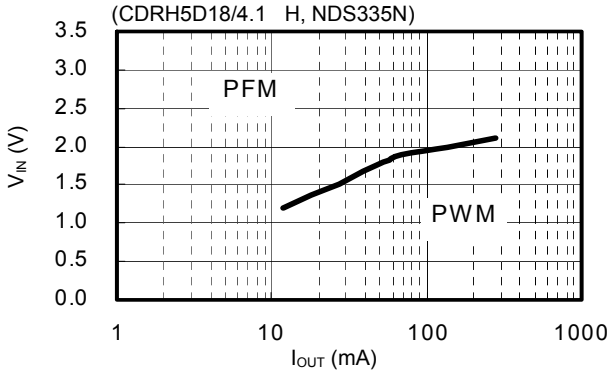


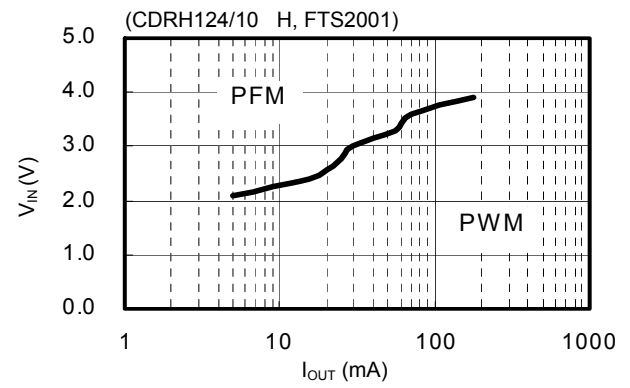
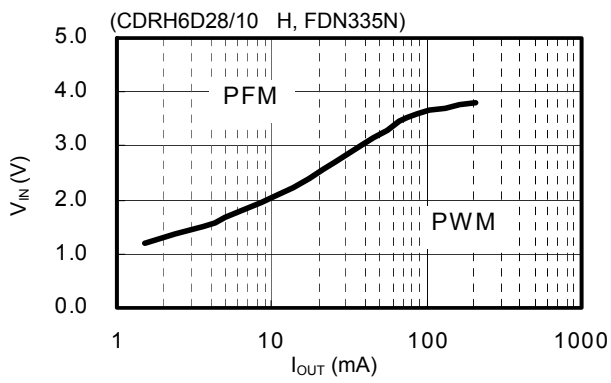
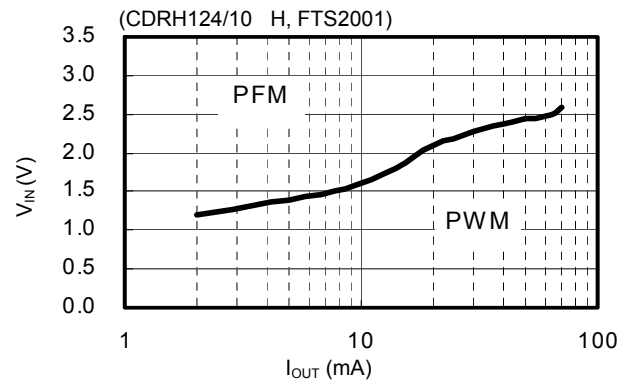
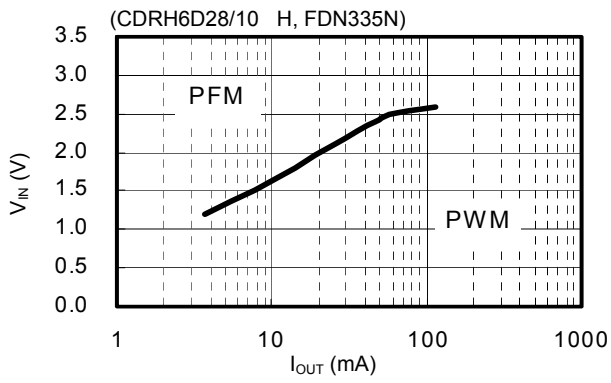




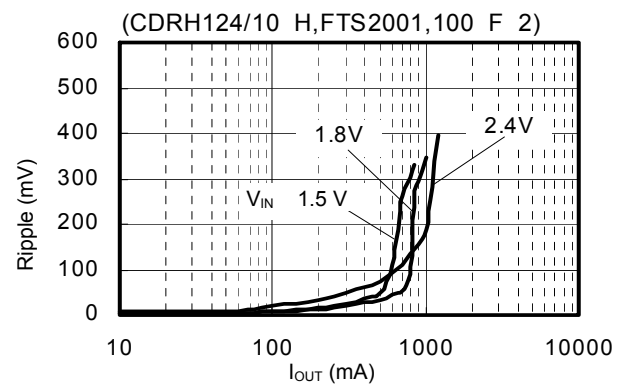
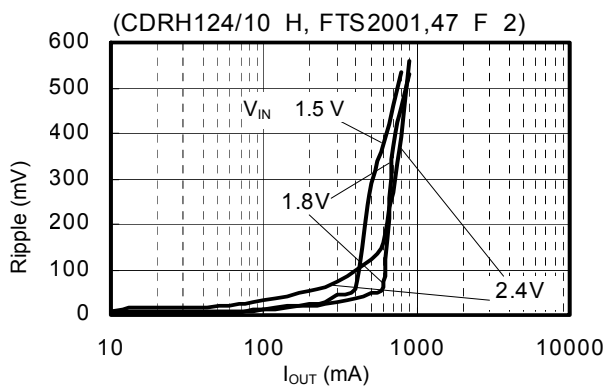
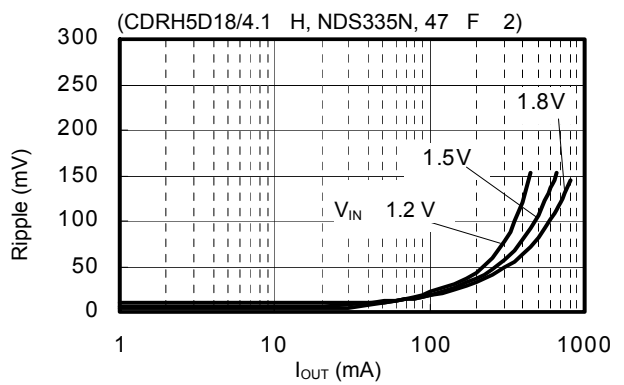
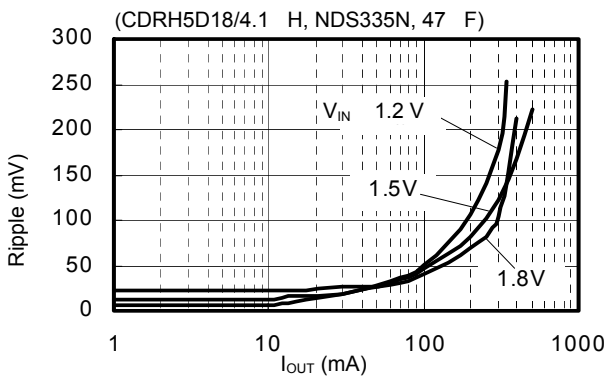
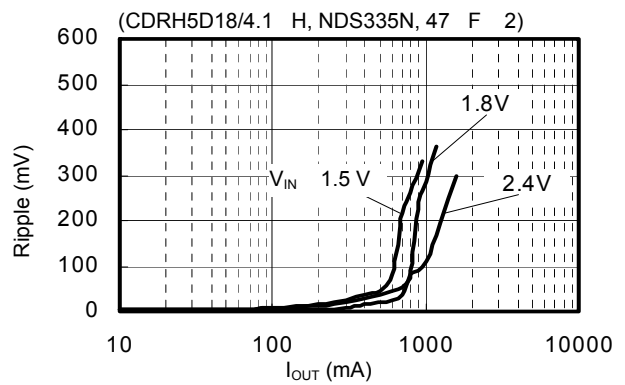
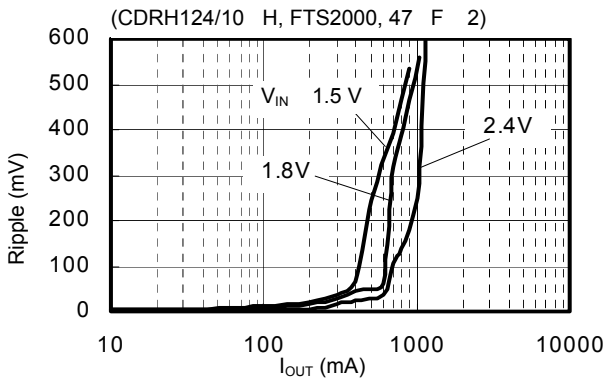
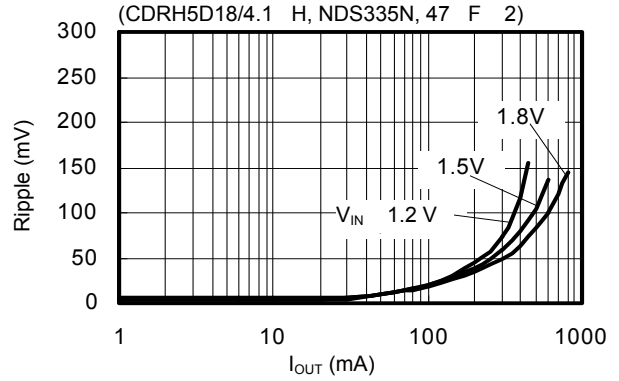
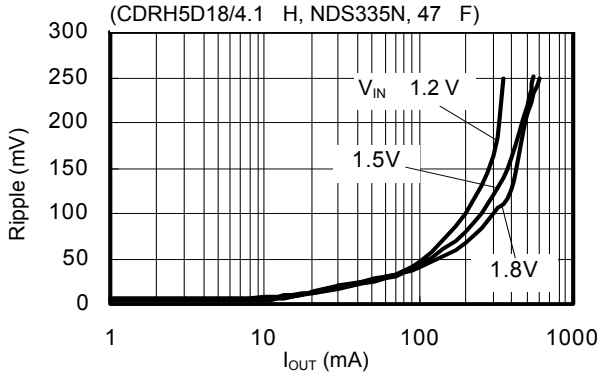


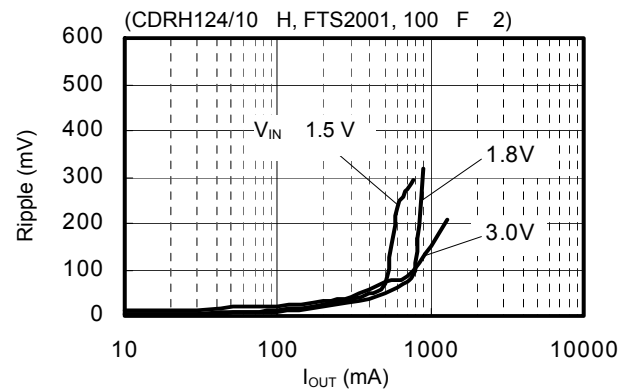
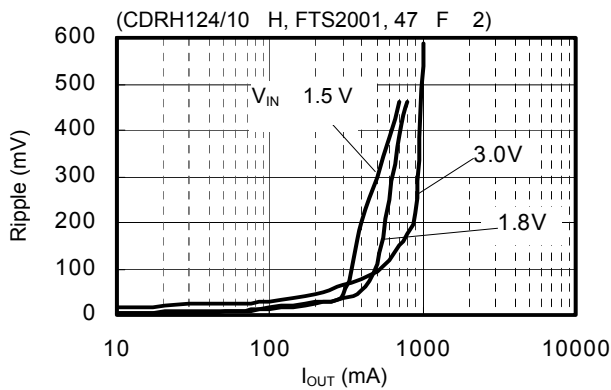
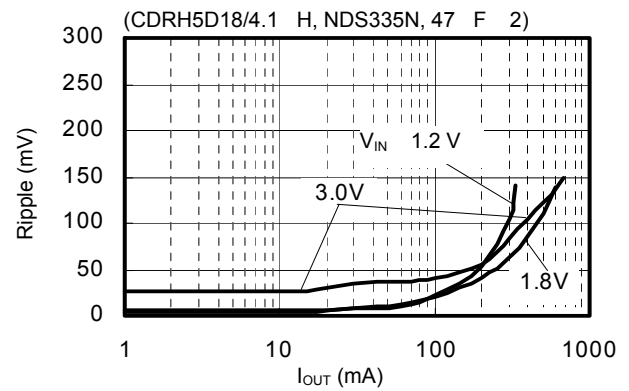
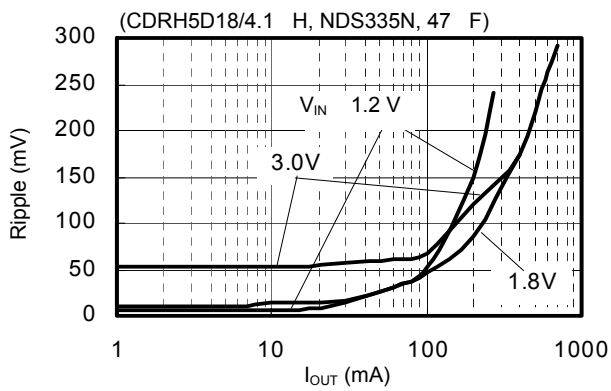
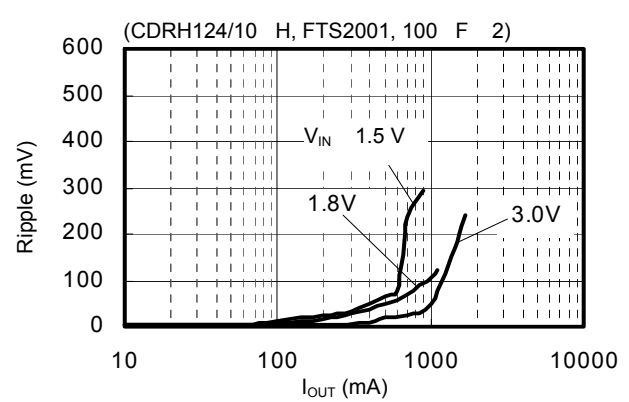
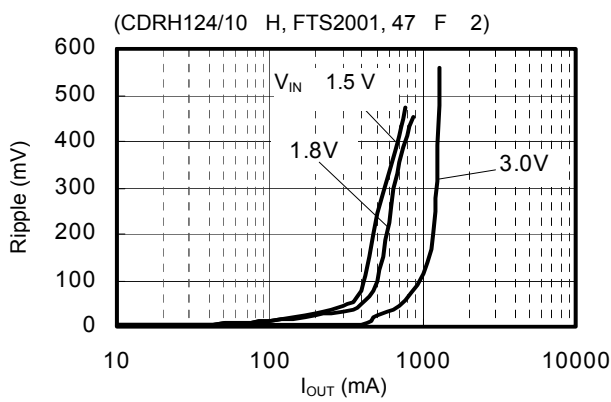
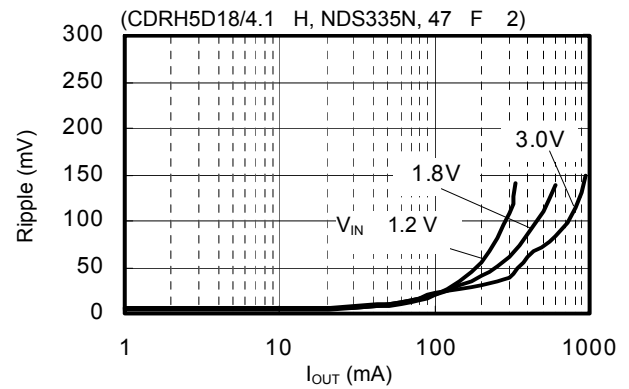
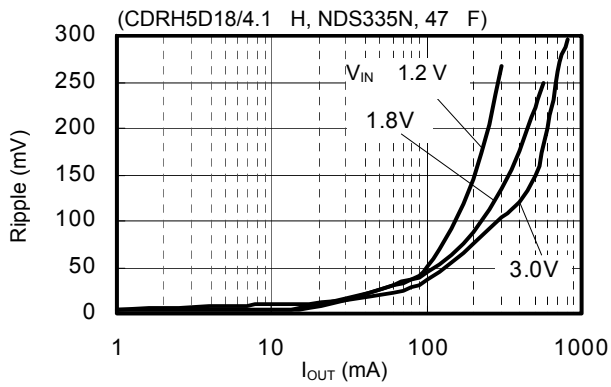
The following shows the actual output current ( $I_{OUT}$ ) vs. PFM/PWM switching input voltage ( $V_{IN}$ ) characteristics when the S-8341 Series is used under conditions (25) to (36) in and .

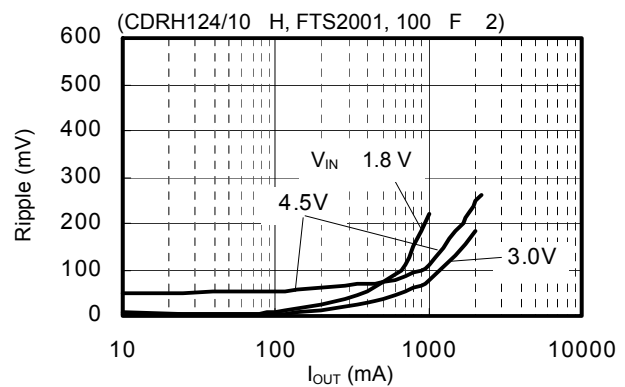
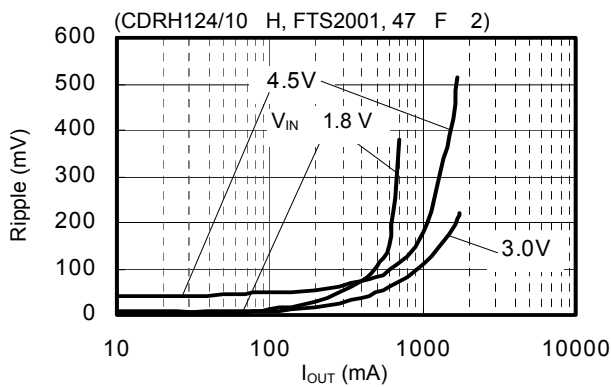
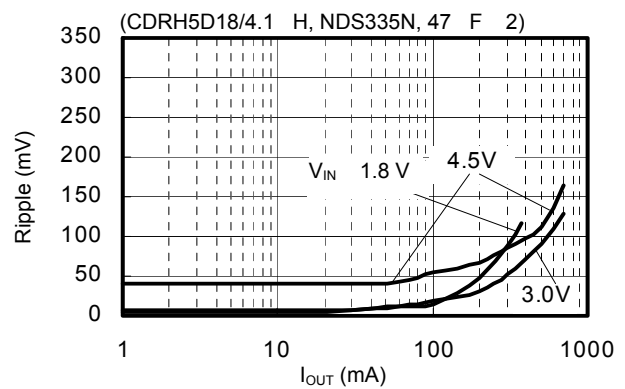
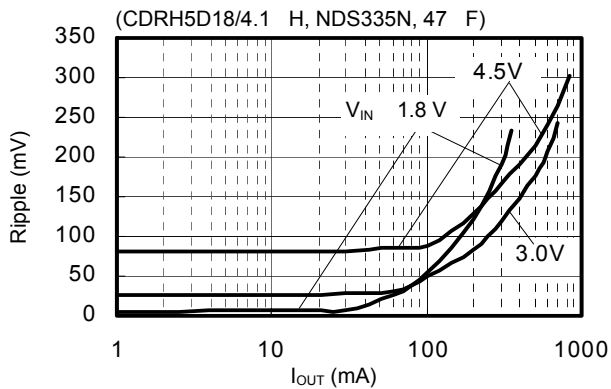
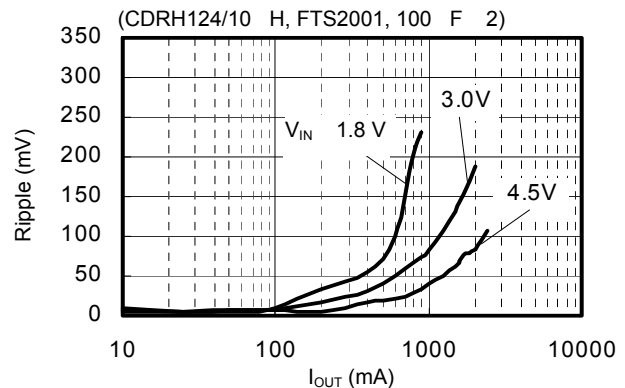
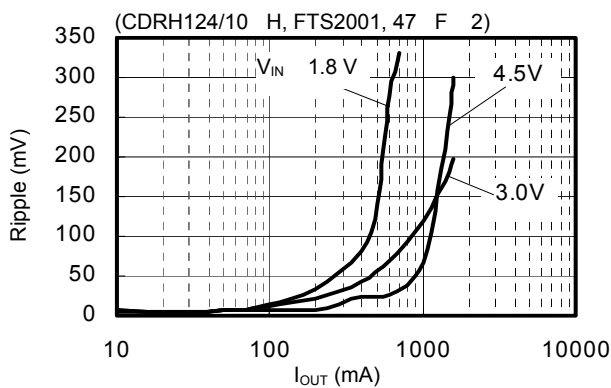
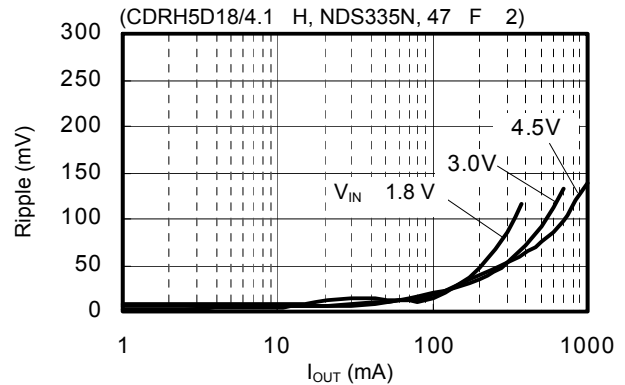
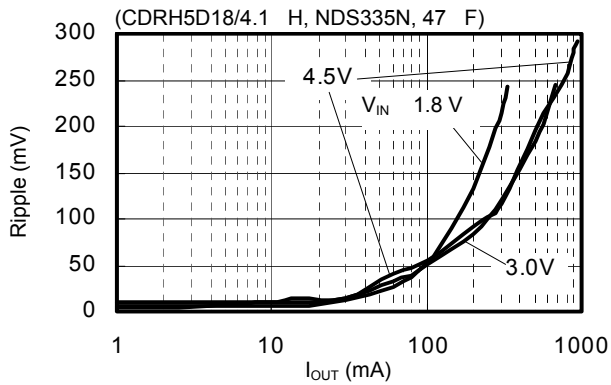


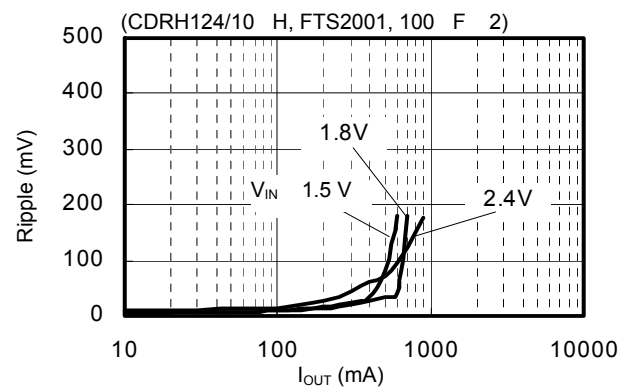
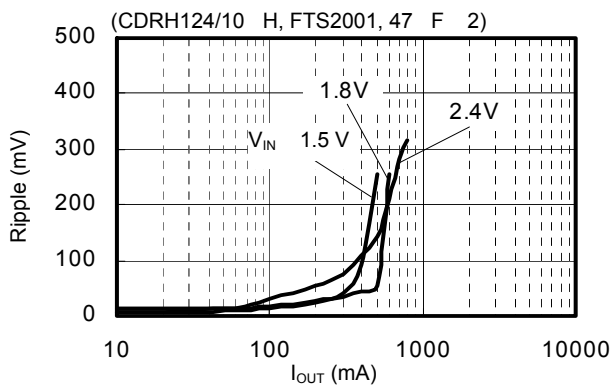
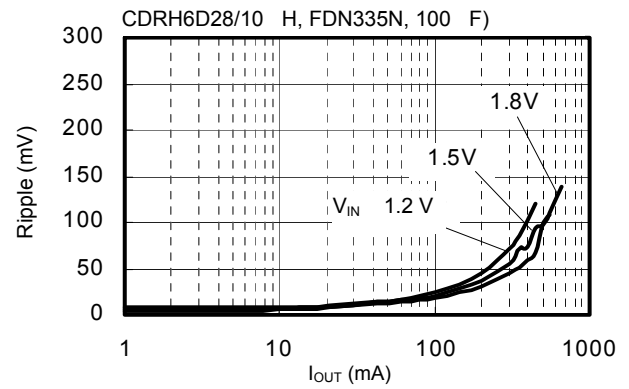
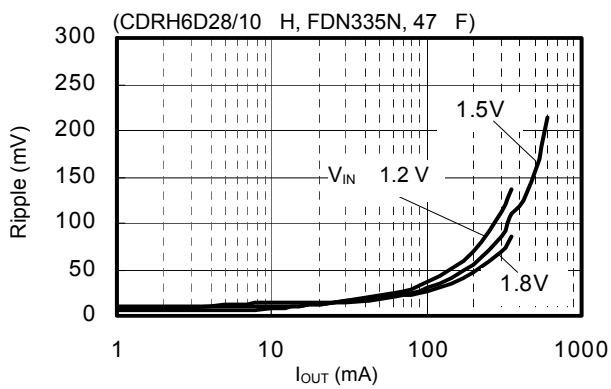
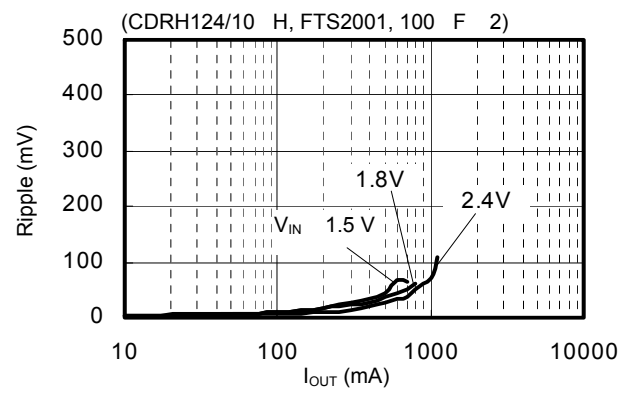
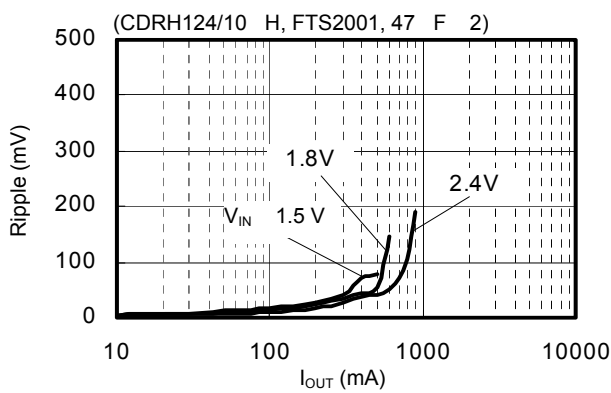
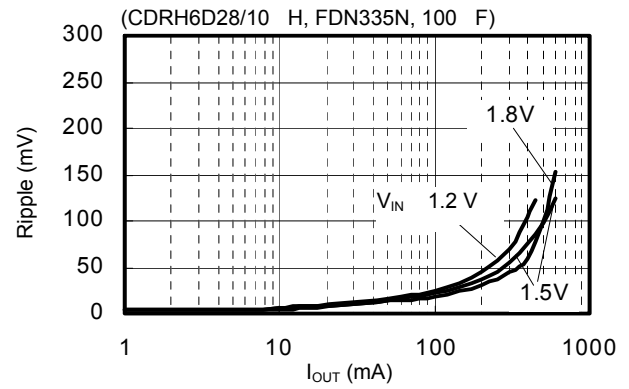
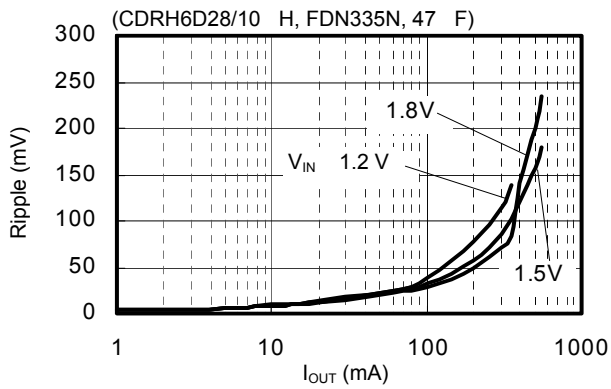


The following shows the actual output current ( $I_{OUT}$ ) vs. ripple voltage (Ripple) characteristics when the S-8340/8341 Series is used under conditions (37) to (60) in .

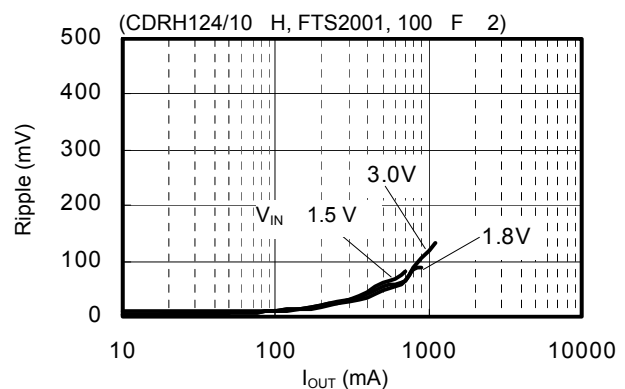
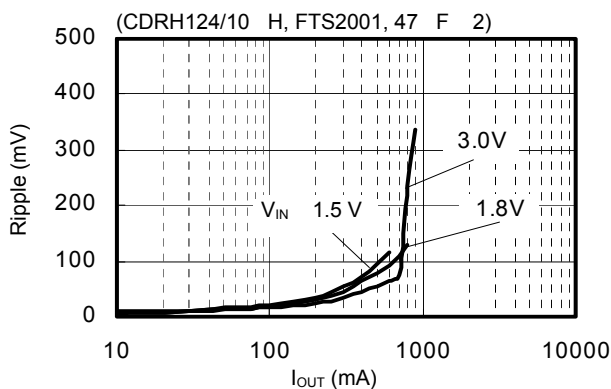
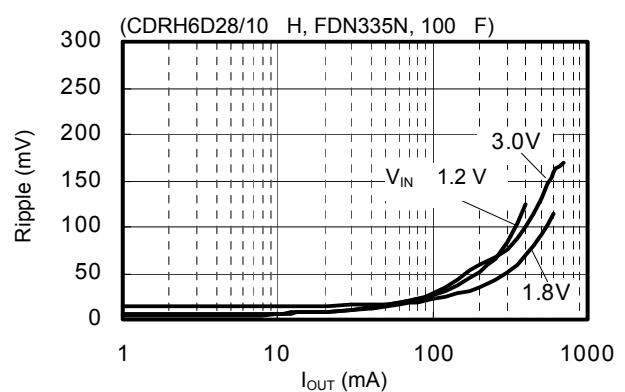
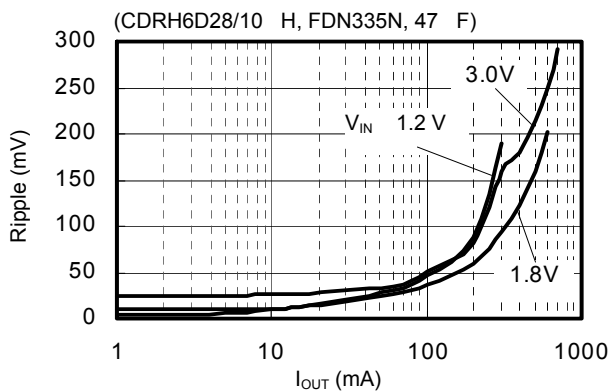
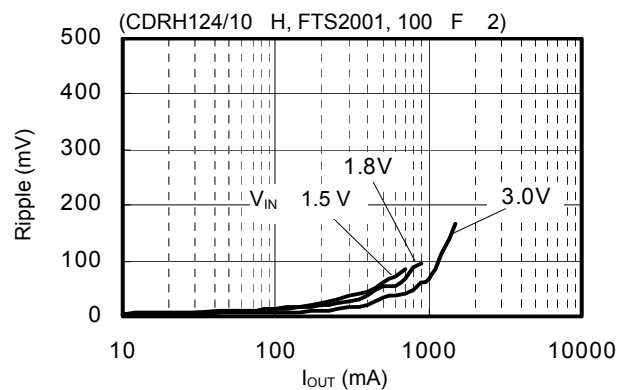
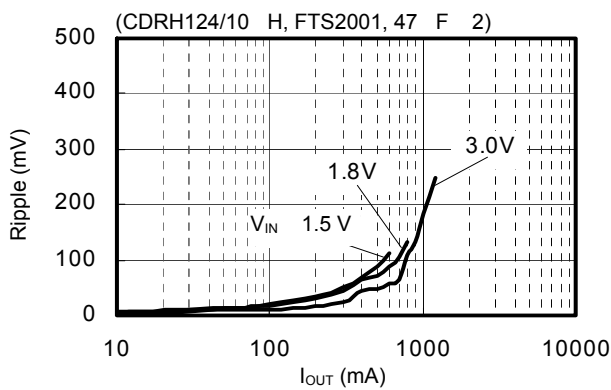
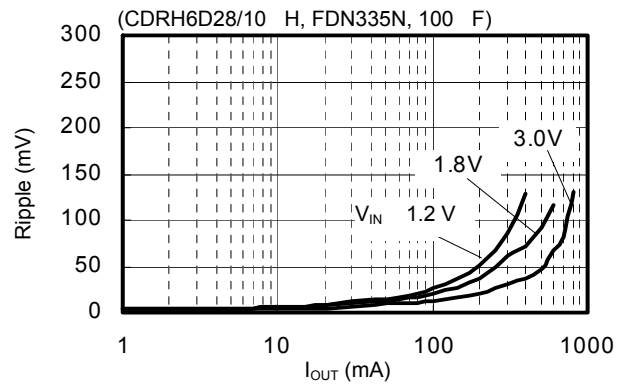
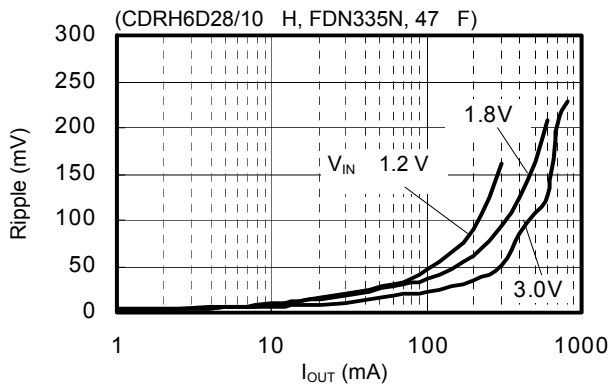


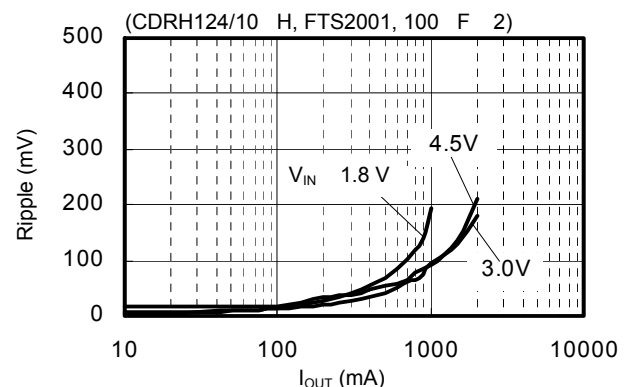
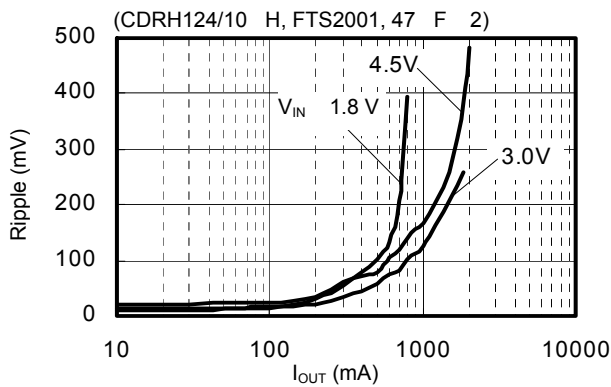
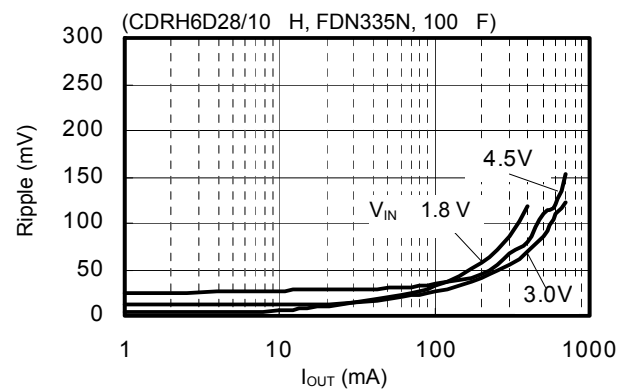
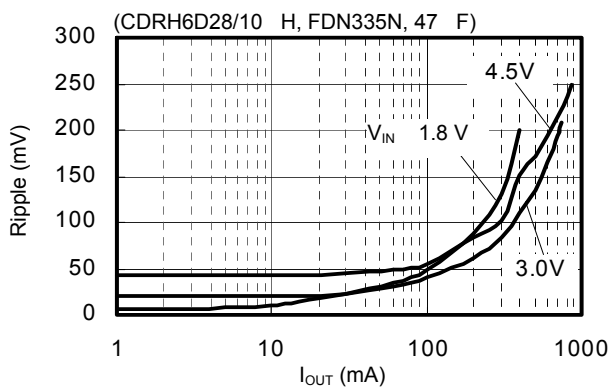
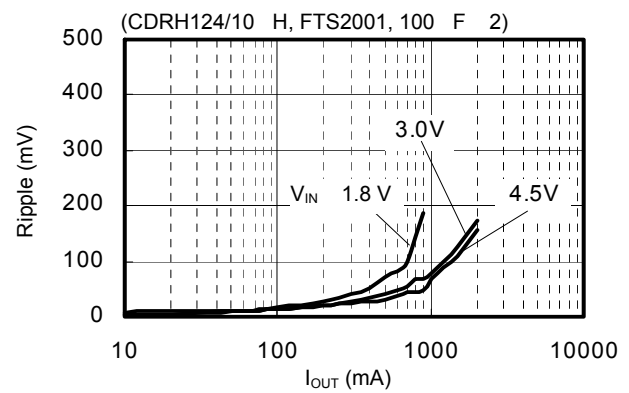
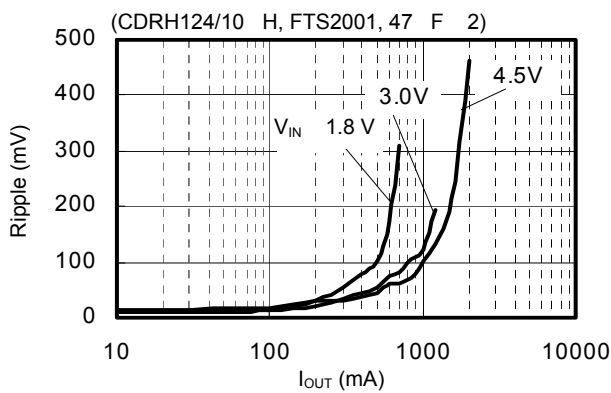
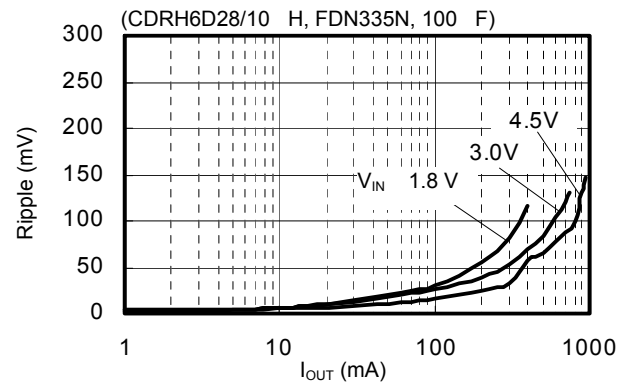
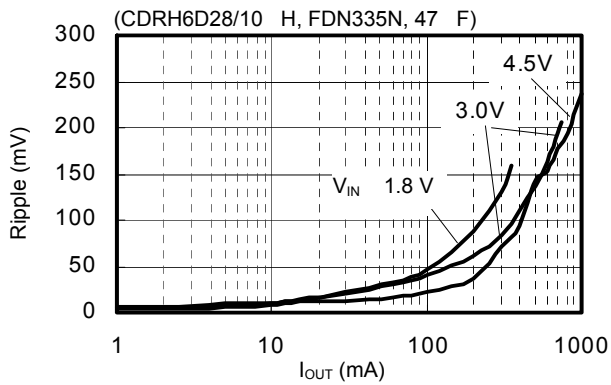


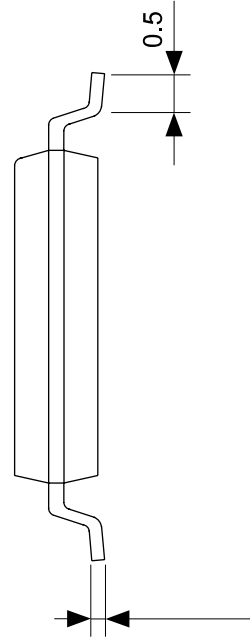
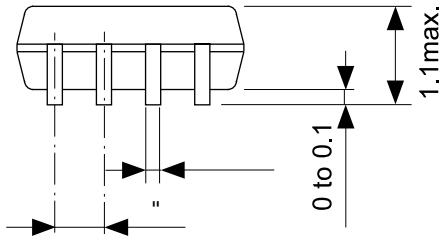
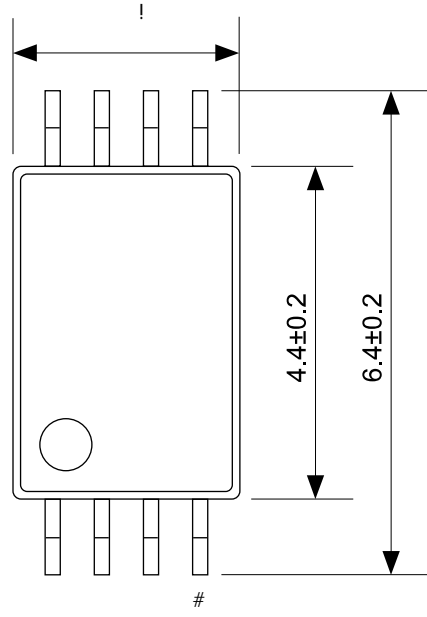




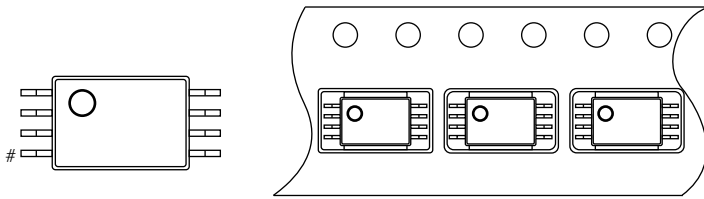
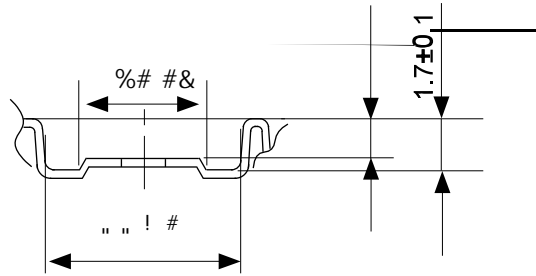
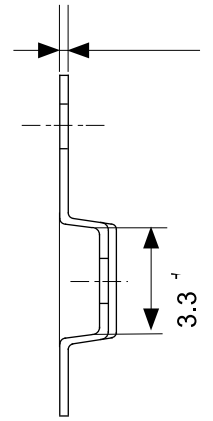
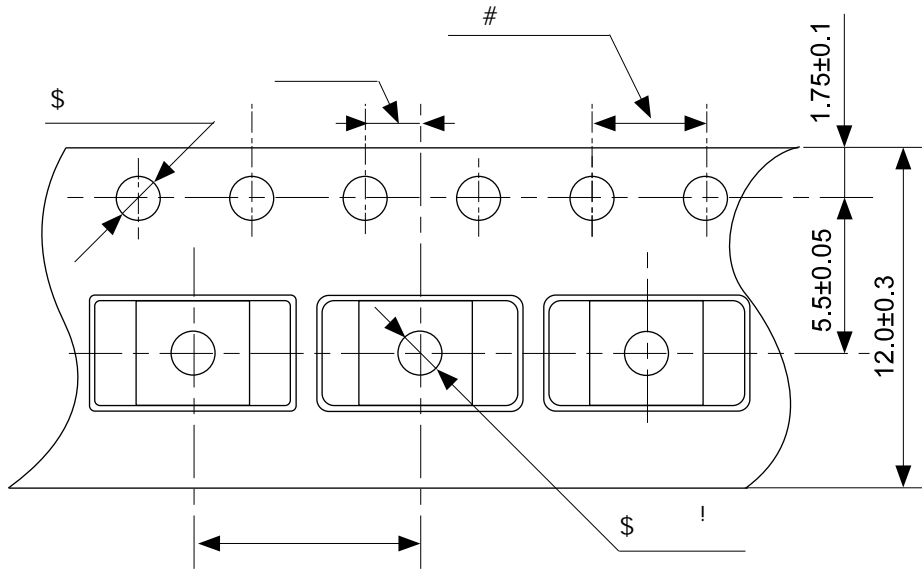








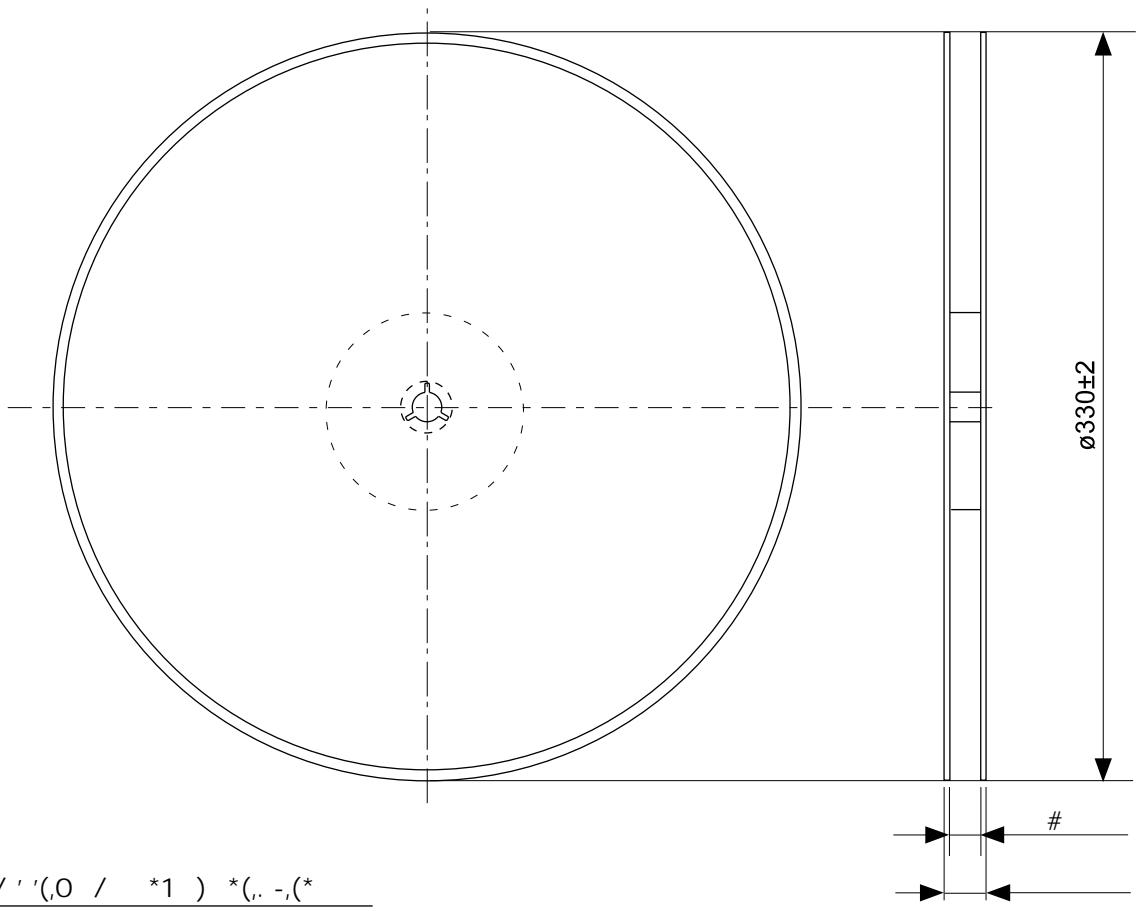
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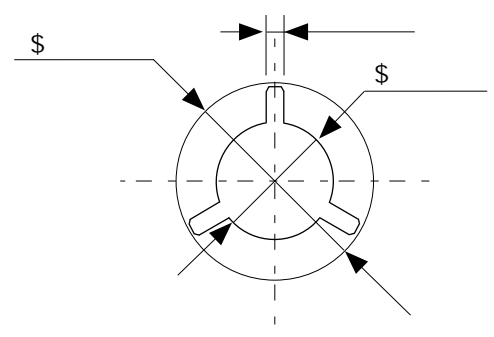
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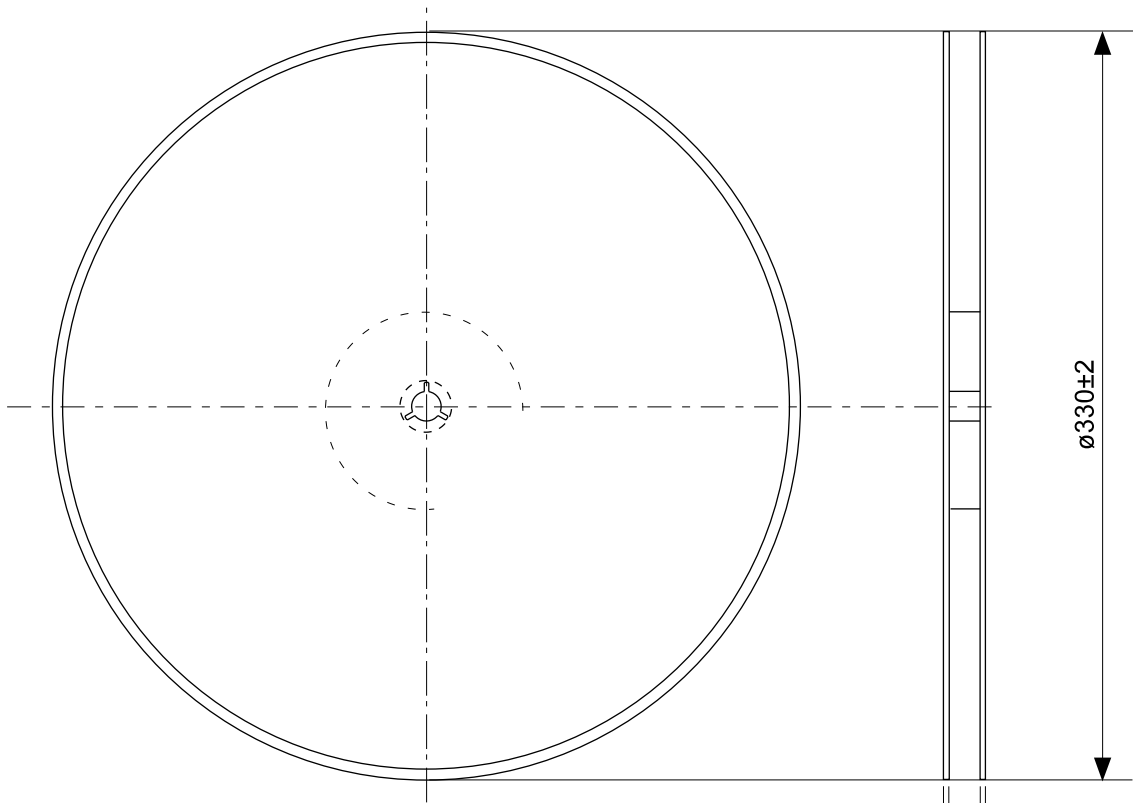


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